

The Effect of Milling Time on the Mechanical Properties of ZA27/Al₂O₃ Nanocomposites

Muslim Çelebi, Aykut Çanakçı*, Serdar Özkaya, A. Hasan Karabacak

Department of Metallurgical and Materials Engineering, Karadeniz Technical University, Turkey

Copyright©2018 by authors, all rights reserved. Authors agree that this article remains permanently open access under the terms of the Creative Commons Attribution License 4.0 International License

Abstract In this study, ZA27/Al₂O₃ nanocomposites reinforced with 1 vol.% Al₂O₃ nanoparticles were produced using mechanical milling and hot pressing method. The milling time was changed between 1h to 8h. The hot pressing process was performed in vacuum at 432^oC and pressure of 600 MPa. The effect of milling time on the density, hardness and tensile strength of the ZA27/Al₂O₃ nanocomposites were investigated. The results show that the increase in milling time resulted as a decrease in the density of nanocomposite due to the change in hardness of that. It was observed that the tensile strength of the nanocomposites reached their maximum value (163 MPa) at milling time of 2h and then decreased linearly with increasing milling time. Moreover, the hardness of the nanocomposite milled for 8h was obtained as 155 HB which is about 9 % higher than the hardness of nanocomposite milled for 1h. A linearly increase was also observed the hardness of nanocomposites.

Keywords Al₂O₃, Nanoparticle, Nanocomposite, ZA27, Tensile Strength

1. Introduction

Metal matrix composites (MMC) have received considerable interest in researches due to their favourable properties such as high strength, high stiffness, superior wear resistance, and retention of strength at room [1] and elevated temperatures [2]. The addition of ceramic reinforcements into the metal matrix can make the composites have enhanced wear resistance, strength and stiffness compared the monolithic materials [1]. They have been widely used in the areas of aeronautical, aerospace, automotive, mechanical, and electronics [2]. Zn–Al based metal matrix composites have been known for their good combination of physical, mechanical and technological properties. Their remarkable characteristics are high strength, low melting point, good castability and machinability, excellent tribological properties and low

manufacturing cost. This material has shown satisfying service performance at engineering applications where strength, hardness, low weight, wears and corrosion resistance, or good pressure tightness is required [3-5].

Of the newer alloy, ZA27 is of particular interest due to their superior properties such as high strength, excellent wear resistance and good corrosion resistance. This alloy has high values of tensile strength up to 450MPa at ambient temperature [6]. Because of their lower cost and equivalent or superior performance, it has been used in bearing and bushing applications as a replacement for bronze bearings [7-9]. However, the main restriction of the ZA27 alloys is that they are not favourable to use above to 100 °C due to defect of their mechanical properties. Hence, adding the hard ceramic particles into the ZA27 matrix alloy is good way to improve their mechanical characters [10].

There are various fabrication techniques available in the production of the MMC materials, including powder metallurgy, stir casting, thixomolding, liquid metal infiltration and squeeze casting [11]. The most commonly method is stir casting but, in this method, the distribution of reinforcement in the matrix is not enough to obtain the required properties of MMC. The dispersion of the powders must be homogenous in the composite material for an effective composite component. A good wettability of reinforcement materials with the matrix materials is another important point. The better wettability with matrix material provides the better properties of composite. Because of this reason, it can be mentioned about a new method, mechanical alloying [12-14]. The control of process parameters, ability to produce a several of materials and high flexibility can be ensured with mechanical alloying. Besides, in this method, the powder particles are being milled using ball collisions which enable to obtain very fine particle size and homogenous distribution. Mechanical alloying is known as a beneficial method for making distribution of the reinforcement particles better in composites before the forming of them with hot pressing [15].

There are varied studies concentrate on metal matrix nanocomposites especially on aluminium and magnesium

based nanocomposites. But the investigation on Zn based nanocomposites was not studied enough. The purpose of the present work was to investigate the effect of milling time on the physical and mechanical properties of ZA27/Al₂O₃ nanocomposites.

2. Experimental Details

Al₂O₃ nanoparticle (1 vol.%) was used as reinforcement particle. The ZA27 powders with average particle size of about 40,2 μm and Al₂O₃ powders (Graphene Future, Ankara, Turkey) with particle size of 100 nm were used. ZA27 alloy powders were produced by gas atomization process (İki-El Metal Tozlari A.Ş., Turkey). The chemical composition of ZA27 alloy was given in the Table 1. The composite powders were milled by a planetary ball mill (Retsch PM PM 100) at different milling times (1, 2, 4, 6 and 8 h). A ball to powder weight ratio of 5:1 was kept constant in the tungsten carbide vials. Methanol (2 wt.%) was used as a process control agent to overcome the coldwelding and agglomerations. The rotational speed of ball mill was fixed to 300 rpm. The parameters for mechanical milling and initial material properties were given in Table 2.

The milled composite powder mixtures were put into a steel die and cold pressed at 300 MPa and then hot-pressed at 432 °C and a pressure of 600 MPa. The graphite and zinc stearate were used for decrease to friction between powders and inner wall of steel die.

The density of nanocomposite samples was determined by the Archimedes method. Theoretical densities of nanocomposites were calculated using rule-of-mixture. The porosity was calculated by using the theoretical and experimental densities.

Brinell hardness values (HB) were measured on the polished samples using a ball with 2.5 mm diameter at a load of 62.5 kg. Each data point of hardness was an average value of not less than five measurements.

The tensile tests were conducted in MTS Criterion Universal testing machine (ASTM A370) at room temperature with a loading speed of 5 mm/min. The average strength values of three specimens were obtained for the nanocomposites.

3. Result And Discussions

3.1. Morphological and Microstructural Investigations

The morphological and microstructural investigations of milled powders and consolidated samples are shown in Fig.1. respectively. As shown in the figure, the powder morphologies of milled powders are changing with increasing milling time from angular to flake powder morphology. In the initial milling times (1h), it is clear that the powder morphology is angular. However, the powder morphology turns into flake morphology with increasing milling time. The reason of this transform is the collisions between milling balls and powders. In the early stage of milling, the alloy powders are fractured from the edges (1h and 2h). After 4 hours of milling, it is clear that the powders were fractured from the edges and the morphology looks flake shape which is going on up to 8h of milling. Further more, when investigate the microstructure of bulk samples we can see that, the Al₂O₃ particles were distributed homogenously for all milling durations. As seen in the figure, due to the fact of being relatively small particles, most of the Al₂O₃ particles are located in grain boundaries.

Table 1. Composition of ZA27 alloy in weight percent (ASTM B669-82)

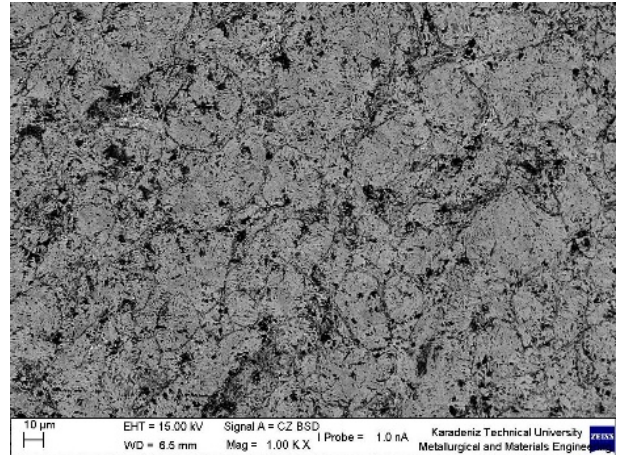
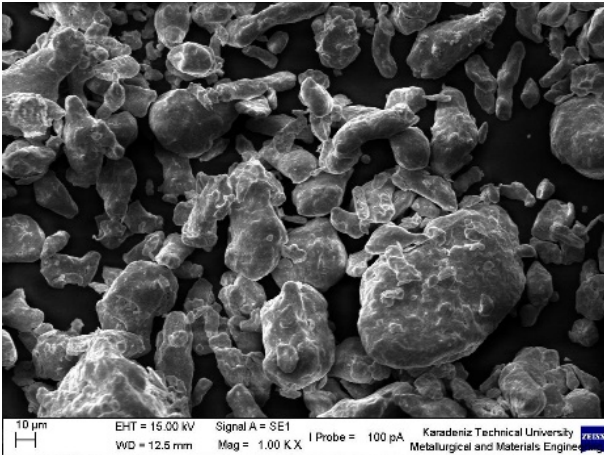
Component	Aluminium	Magnesium	Copper	Zinc
Percentage Composition	25-28	0,01-0,02	2,0-2,5	Balance

Table 2. The properties of as-received materials and milling parameters.

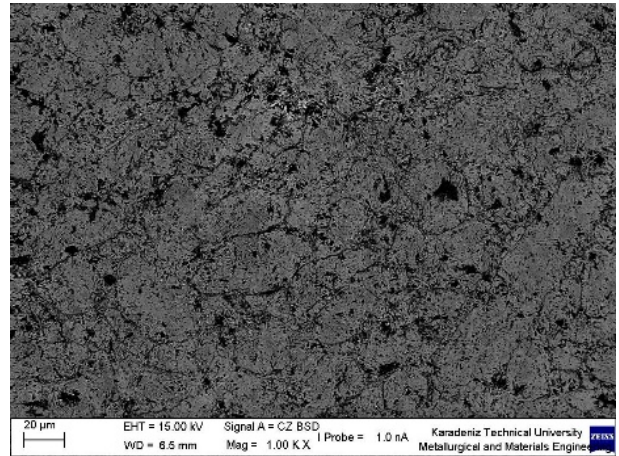
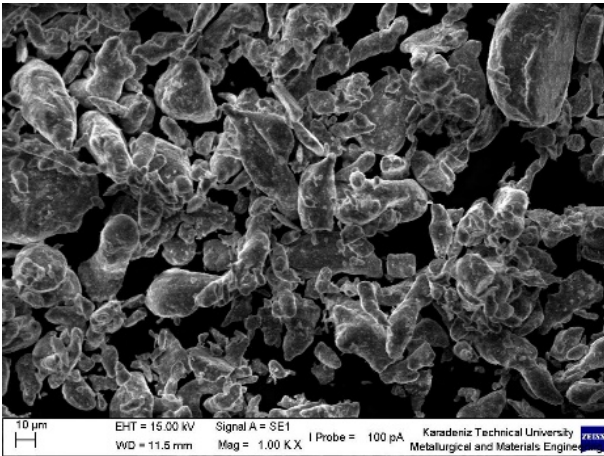
Material	Composites designation		Milling Parametres			PCA (wt.%)	Milling time (h)	Sample code
	ZA27 particle size (μm)	Al ₂ O ₃ content (%)	Al ₂ O ₃ particle size (nm)	Milling speed (rpm)	BPR			
ZA27-Al ₂ O ₃	40,2	1	100	-	-	-	0	S0
ZA27-Al ₂ O ₃	40,2	1	100	300	5:1	2	1	S1
ZA27-Al ₂ O ₃	40,2	1	100	300	5:1	2	2	S2
ZA27-Al ₂ O ₃	40,2	1	100	300	5:1	2	4	S3
ZA27-Al ₂ O ₃	40,2	1	100	300	5:1	2	6	S4
ZA27-Al ₂ O ₃	40,2	1	100	300	5:1	2	8	S5

Powder

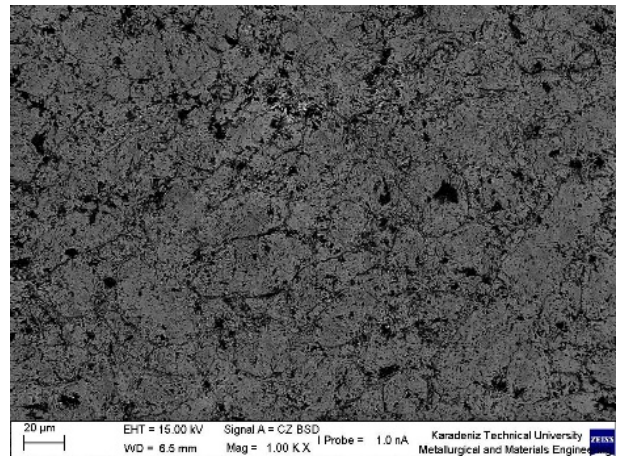
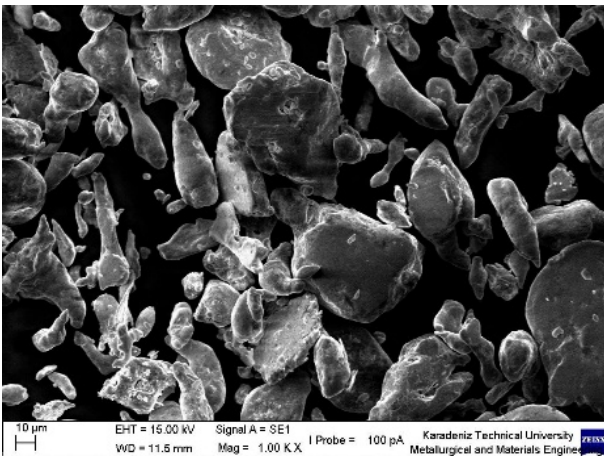
Bulk Sample



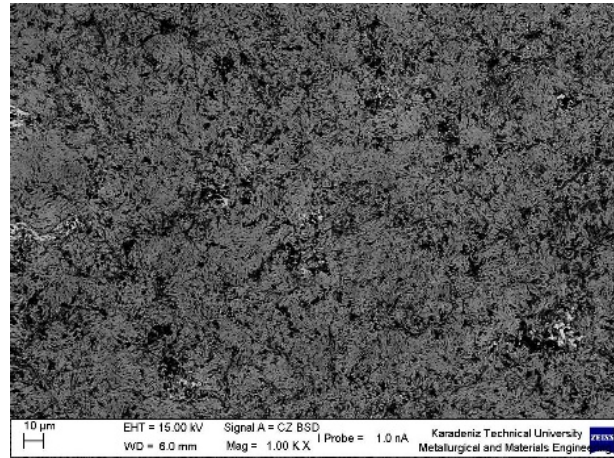
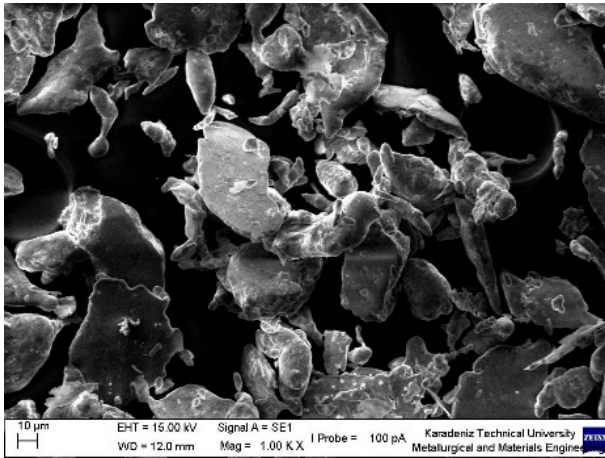
1h



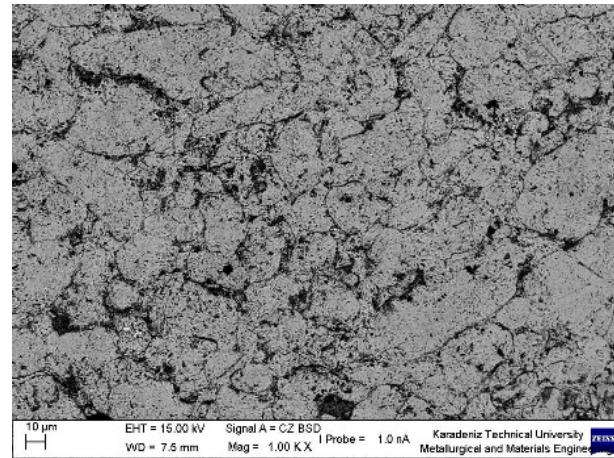
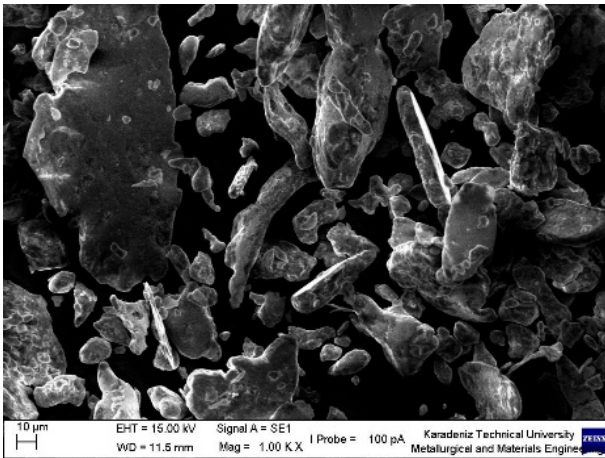
2h



4h



6h



8h

Figure 1. Powder morphology and microstructure evolution related to milling time

3.2. Density and Porosity

The experimental densities and porosities of ZA27/ Al_2O_3 nanocomposites was shown in Figure 2. The results showed that increase in milling time result in porosities of nanocomposites. The reason for increasing in porosity as a function of increasing milling time can be explain by the work hardening effect of milling process. During milling process, the mixed powders are subjected to the high energy collisions between ceramic particles and milling balls which result in higher hardness of powders. While the hardness of powders increases the compressibility of powder decreases as a result of increased compressibility resistance of particles. It can be seen in figure 1 that increasing milling time was caused an increase in porosity also a decrease in density. As compared the densities of S1 sample to S5 sample, the density of S1 sample was about 2,5% higher than the density of S5 sample. It can be said that the milling time was not have a great effect on the densities of ZA27/ Al_2O_3 nanocomposites because the difference in densities of

nanocomposites was very low. The highest porosity was seen in S5 sample which is about %200 higher than S1 sample.

3.3. Hardness

Severe plastic deformation, which occurs during the milling process, leads to the increase in the hardness of milled ductile powders. Figure 2 shows the hardness values of nanocomposite samples. As the milling time was changed from 1 to 8h, the hardness of samples was increased substantially. As seen in Fig.3, the hardness of the nanocomposites was increased dramatically after milling time of 2h. While the hardness value of S1 sample (milled for 1h) was 142,3 HB, it was increased to 149 HB at S5 sample (milled for 8h) which is about %5 higher than S1 sample. This can be attributed to the work hardening effect of milling process. The nanocomposite powders undergo more plastic deformation with increasing milling time and this effect increases the hardness of powder and hence the hardness of nanocomposites.

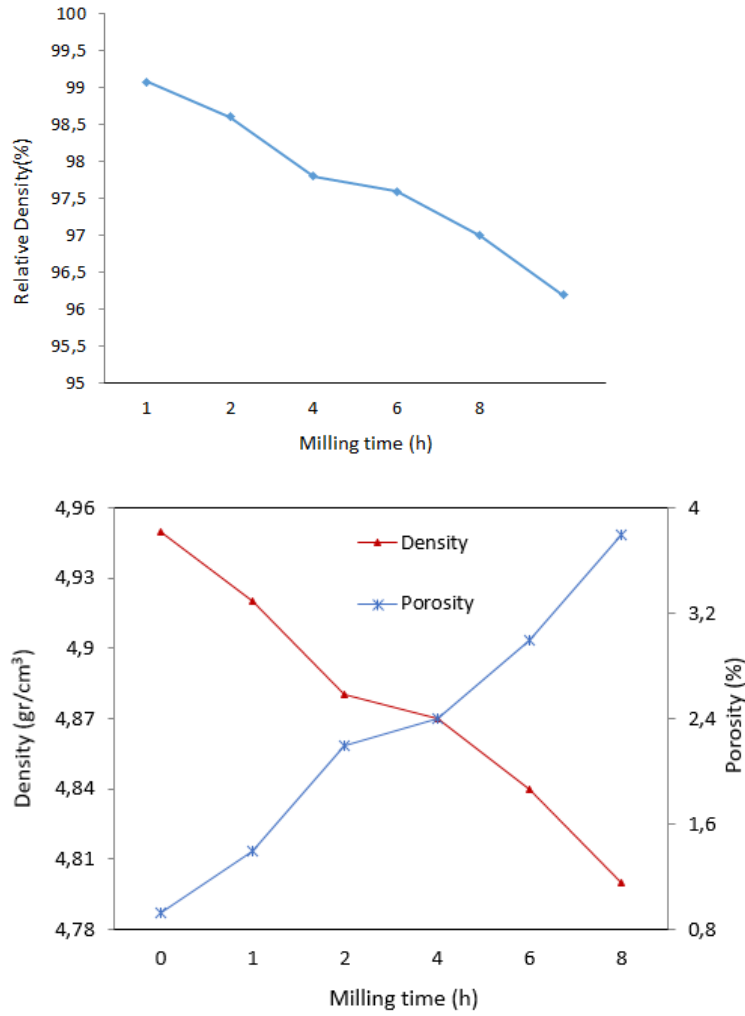


Figure 2. The density and porosity of nanocomposite samples

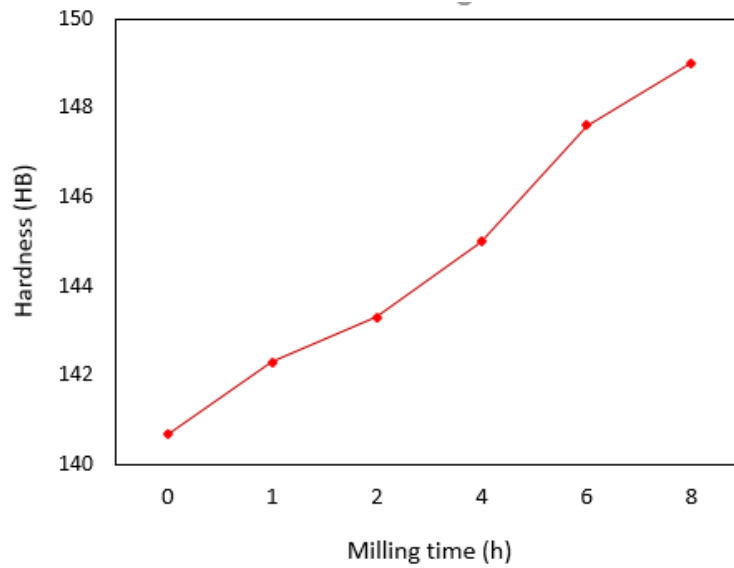


Figure 3. The hardness of nanocomposite samples

3.4. Tensile Strength

In the attempt to better evaluate mechanical properties of nanocomposites, tensile tests were conducted at room temperature and the results of test were shown in Figure 4. It can be seen that for the initial stages of milling up to 2h milling time, the increasing in milling time provided an increase in tensile strength of nanocomposite. This increase can be explained with the increasing in powder hardness and decrease in powder size. During the milling process the collisions between powder particles and ball mill results as increase in powder hardness. Thus, the tensile strength of bulk samples also increased because of increasing hardness of raw materials. However, after 2h milling the tensile strengths were rapidly decreased because increasing the ball-milling led to more work hardening effect which makes the nanocomposites brittle. This is an expected situation when working with ductile alloy powders. In the initial stage of milling, the tensile strength of composite increases but when continue to the milling the powder characteristic turns into brittle from ductile structure which results as a sudden decrease in tensile strength. While the highest tensile strength was obtained 210 MPa at S2 sample, the lowest value was obtained 139 MPa at S5 sample. Comparing to milling time of 2h, the tensile strength was decreased about 30% at the end of milling time of 8h.

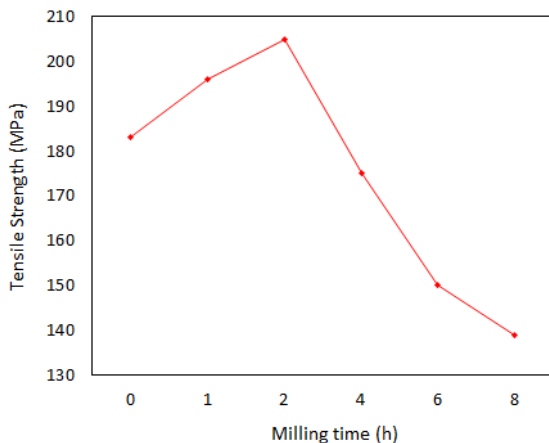


Figure 4. The tensile strength of nanocomposite samples

4. Conclusions

- Increase in hardness of nanocomposites was observed with increase in milling time.
- Porosity and density measurements showed that increasing milling time caused a decrease in density and increase in porosity.
- Increase in milling time resulted in decrease in tensile strength of nanocomposite up to 2h of milling, on the other hand after 2h milling they suddenly decrease.

Acknowledgements

This work was supported by ‘The improving of nanoparticle reinforced Zn-Al based nano-composite materials by mechanical alloying method, the investigation of their microstructure-mechanical and tribological properties’ named and 213M276 numbered ‘Scientific and Technological Research Council of Turkey’ 1001 project.

REFERENCES

- [1] J. S. Yang, Y. H. Park, B. G. Park, I. M. Park and Y. H. Park. 2013. Microstructure and mechanical properties of Alborex+SiCp/AS52 hybrid metal matrix composites, *International Journal of Cast Metals Research*, 21:1-4, 231-234.
- [2] Varol, T., et al. (2015). "Modeling of the Prediction of Densification Behavior of Powder Metallurgy Al-Cu-Mg/B4C Composites Using Artificial Neural Networks." *Acta Metallurgica Sinica-English Letters* 28(2): 182-195.
- [3] Zhu, Y.H., Man, H.C., Lee, W.B., 2003. Microstructure of laser melted Zn-Al-based alloy. *J. Mater. Process. Technol.* 139 (1-3), 296-301.
- [4] Savaskan, T., Hekimoglu, A.P., 2014. Microstructure and mechanical properties of Zn-15Al-based ternary and quaternary alloys. *Mater. Sci. Eng. A* 603, 52-57.
- [5] Bobic, B., Bajic, N., Jovanovic, M.T., Bobic, I., 2009. Microstructure and mechanical properties of Zn₂₅Al₃Cu based composites with large Al₂O₃ particles at room and elevated temperatures. *Metall. J. Mater. Eng.* 15 (4), 245-255.
- [6] Muthukumarasamy S, Buni BY and Seshan S. ZA27 alloy-based cast MMCs with ceramic reinforcement. *AFS Transactions*. 1994; 102:819-824.
- [7] Ranganath G, Sharma SC, Krishna M, Muruli MS. A Study of mechanical properties and fractography of ZA-27/titanium-dioxide metal matrix composites. *JMEPEG* 2002;11:408-13
- [8] Sharma SC, Girish B, Kamath MR, Satish BM. Graphite particles reinforced ZA-27 alloy composite materials for journal bearing applications. *Wear* 1998;219: 162-8.
- [9] Li Y, Ngai TL, Xia W, Zhang W. Effects of Mn content on the tribological behaviors of Zn-27% Al-2% Cu alloy. *Wear* 1996;198:129-35
- [10] Girish, B.M., Prakash, K.R., Satish, B.M., Jain, P.K. and Devi, K., Need for optimization of graphite particle reinforcement in ZA-27 alloy composites for tribological applications, *Materials Science and Engineering A*, 382-388, 2011.
- [11] C.H. Fan, Z.H. Chen, W.Q. He, J.H. Chen, D.J. Chen, J. Alloys Compd. 504, 42 (2010)

- [12] Dzunic, M., Mitrovic, S., Babic, M., Bobic, I., Pantic, M., Adamovic, D. and Nedeljkovic, B., Nanoindentation of Za-27 Alloy Based Nanocomposites Reinforced with Al₂O₃ Particles, Tribology in industry, 413-420, 2015.
- [13] Mitrovic, S., Babic, M., Bobic, I., Dzunic, D. and Jeremic, B., Tribological Behavior of Composites Based on Za-27 Alloy Reinforced with Graphite Particles, 401-410, 2010.
- [14] Casati, R. and Vedani, M., Metal Matrix Composites Reinforced by Nano-Particles-A Review, Metals, 65-83, 2014.
- [15] O. Guler, H. Cuvalcı, M. Celebi and A. Canakcı. 2016. Corrosion Behavior Of ZA27/Graphite/Al₂O₃ Hybrid Nanocomposites, Korsem 2016, Bayburt, Turkey. Pp:541-547