

A Study of Specific Down Force Energy and Cutting Depth of Sapphire Substrate Affected by Different Dipping Temperatures of Slurry

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Abstract This article studies the change of specific down force energy and cutting depth of sapphire substrate when sapphire substrates were dipped in different temperatures of slurry. It involved applying small down force in cutting sapphire substrates by atomic force microscope (AFM) before dipping them in slurry in order to obtain the SDFE value of without dipping slurry. Next, small down force was applied to cut sapphire substrates dipped in slurry for varying dipping temperatures to obtain the SDFE_{reaction} values of dipping slurry with different dipping temperatures. Nanocutting was performed by AFM with a small constant down force to obtain the cutting depths of sapphire substrate for the different dipping temperatures of slurry. The results of this study indicated that the dipping temperature of slurry increased, the SDFE_{reaction} value of sapphire substrate decreased and the cutting depth of sapphire substrate with a constant down force increased.

Keywords Specific Down Force Energy, Atomic Force Microscopy, Sapphire Substrate, Slurry Dipping Temperatures

1. Introduction

AFM is generally used for measuring and observing conductive and nonconductive surface patterns. AFM probes can be used as cutting tools and microstructures in semiconductors, optoelectronics, and metal surfaces (Tseng et al. [1]). Fang et al. [2] used AFM probes in scribing experiments involving a Si substrate coated with an Al film, and found that the scratch depth increased with the applied down force on the probe and the number of scribing cycle. The applied down force had the most notable effect. Yan et al. [3] used AFM to establish a similar cutting system based on computer numerical control. They used an AFM

diamond coated probe tip as a cutting tool to scratch Cu film deposited on a Si substrate. Tseng et al. [4] used AFM probe tip to scratch Si wafer, and obtained a regression analysis that showed a logarithmic relationship between the dimension of the nanogroove and the down force of the probe, and a power-law function relationship between the dimension of the nanogroove and the number of scratching cycle. Currently, most studies on nanoscale cutting and scribing use Cu and Al as the cutting materials (Lin and Huang, [5]; Nga et al. [6]). Peng et al. [7] used AFM diamond probe to cut nanoscale groove in an Al film. Kanki et al. [8] investigated the characteristics of CMP and utilized the chemical reaction layer formed by slurry to improve the planarization of the CMP. Various slurry pH values, dipping times, and material electrolytic polarization characteristics were analyzed. Kanki et al. [8] also sliced Cu specimens dipped in slurry, and the thickness of the chemical reaction layer was determined through transmission electron microscopy. In optical semiconductor manufacturing processes, chemical mechanical polishing (CMP) is a key technology for the planarization of wafers. Factors influencing the performance of CMP include the composition, volume concentration, and temperature of the slurry, the rotation speed, down force and polishing pad. The chemical compositions in the slurry induce a chemical reaction with the material surface, generating chemical layer that are softer than the original material and easy to remove. This means that the cutting depth of each abrasive particle will be increased when sapphire substrate dipped in slurry. Therefore, this study analyzed how varying the slurry dipping temperature for sapphire substrate influenced the cutting depth and the value of specific down force.

2. Experimental Apparatus and Method Planning

2.1. Experimental Apparatus and Materials

The Dimension 3100 atomic force microscope (Veeco, Digital Instruments et al. [9]) in the Nano Lab at Tungnan University, Taiwan, was used, Sapphire substrates were used as the experimental material (diameter: 50.8mm (2 in.); thickness: 0.43 mm). AFM diamond coated probe was used to cut straight line groove into the sapphire substrate for observation. The sapphire substrate surface configuration was measured before and after cutting. The AFM probe used in the experiment was a DT-NCHR diamond-coated probe. The thickness of the diamond coat was approximately 100 nm, and the semispherical tip of probe had a sphere radius of approximately 150 nm; thus, the diamond tip of probe was used as a semispherical cutting tool during the experiment.

According to the manufacturer’s instruction manual, the probe has a spring constant of 42 N/m and a resonance frequency of 320 kHz. To obtain a more accurate spring constant k_r , it used AFM in tapping mode to perform a frequency sweep to find the actual resonance frequency f_r of the probe. The spring constant of the probe can be expressed as $k_r = (f_r^2 \times k_v) / f_v^2$. The actual spring constant k_r of the experimental probe was calculated according to the resonance frequency f_r and spring constant k_v provided by the manufacturer and the measured actual resonance frequency f_r (Lin and Hsu et al. [10]). Table 1 shows the resonance frequency and probe spring constant values used in the experiment.

In this study, the slurry was a colloidal silica suspension (pH 9.6, volume concentration: 50%; Allied High Tech Products, Inc.). This slurry is suitable to use in the CMP experiment of polishing sapphire substrate.

2.2. AFM Operation and Down Force Measurement of AFM probe

The AFM contact mode method was employed to accurately measure the down force applied during nanoscale cutting. The force-distance curve method was adopted to measure the applied down force of the probe on the cutted workpiece. The force–distance curve depicts the relationship between the setpoint and the offset of the probe cantilever. In the force calibration mode, the setpoint is the horizontal center of the force–distance curve. The setpoint can be set to obtain the cantilever offset d of the probe under down force. The down force F_d can be obtained using the following equation:

$$F_d = k_r d. \tag{1}$$

To determine the relationship between the setpoint and the down force of the AFM probe applied on sapphire substrate, prior to conducting the experiment, the different setpoints were set with the AFM contact mode. The cantilever offset d at each setpoint was substituted into Equation (1) to obtain the corresponding down force value.

2.3. Dipping Temperature Control Method in Experiment

As for dipping temperature control, first of all, slurry is poured to a beaker, which is then placed on a heating plate. Adjust the button on the heating device to different numerical figures in order to acquire the slurry temperatures required by the study, i.e. 30°C, 40°C and 50°C, as well as room temperature 23°C. In the heating process of slurry, thermometer is used to monitor the temperature. Once the slurry is heated to a specific temperature, the slurry is poured to another beaker, and sapphire substrate is dipped in the heated slurry for 60 minutes. Once the slurry temperature starts to fall, another beaker is used to hold the slurry on the heating plate, and then the slurry is poured to the beaker dipped with sapphire substrate. In the meantime, thermometer is used to monitor the slurry temperature. Through the ways of pouring in the heated slurry and measuring temperature by thermometer, the temperature of slurry is controlled at the required temperature of $\pm 1^\circ\text{C}$, meeting the requirement of the experimental parameter of temperature.

2.4. Experimental Planning

First, the sapphire substrate was dipped in the slurry for 60min at the various dipping temperatures of 23°C, 30°C, 40°C, 50°C. The probe of AFM is used as a tool to cut the sapphire substrate with a down force, then the cutting depths and removed volumes of the sapphire substrate at different slurry dipping temperatures can be obtained. The equation of specific down force energy was used to obtain the values of SDFE without dipping slurry and SDFE_{reaction} at the various dipping temperatures of slurry. Finally, a small constant down force of AFM is used to cut the sapphire substrate to obtain the cutting depths of sapphire substrate at the various dipping temperatures of slurry.

Table 1. Resonance frequency and probe spring constant used in the experiment

f_r (measured resonance frequency)	385 kHz	k_r (actual probe spring constant)	60.8 N/m
f_v (manufacturer-provided resonance frequency)	320 kHz	k_v (manufacturer-provided probe spring constant)	42.0 N/m

3. SDFE Theoretical Model and Calculation Method

The study considered that during the actual nanocutting process, down force is applied when the probe exerts sufficient downward force to achieve a certain depth in the workpiece for cutting in the cutting direction. The specific down force energy, SDFE, is defined as following equation (2) (Lin and Hsu et al. [9]):

$$\text{SDFE} = \frac{F_d \times \Delta d_n}{\Delta V_n} \quad (2)$$

where F_d is the down force exerted by the probe tool, Δd_n is the increase in cutting depth for cutting pass n , and ΔV_n is the volume removed from the workpiece for cutting pass n . Because the change in volume is relative to the increase in cutting depth, ΔV_n is a function of Δd_n .

In this study, it assumed that with the same workpiece material, the SDFE would be relatively constant. Additionally, because the probe tip was a semispherical cutting tool, the volume removed from the workpiece during the first cutting pass was determined using a geometric formula for spheres. Grooves were created in each cutting pass by pressing the semispherical cutting tool into the workpiece in a linear motion. Observation of the groove configuration after the cutting experiment indicated that the probe tool initially penetrated the workpiece at a shallow depth; as the probe tool moved to an intermediate region, the cutting depth increased to a fixed value, thus increasing the removal volume. Therefore, to ensure that the cutting depth was in line with actual machining conditions, the average cutting depth was measured and calculated based on the intermediate region of the groove.

As mentioned, the volume of material removed on the first cutting pass was the volume of a spherical cap initially. At this point, the down-force removed volume is the volume of the spherical cap of the probe tip. The depth gradually became fixed after the tool was moved to the intermediate region of the cutted groove. Of the volume

removed by the applied down force of the moving probe tip, the volume with a distance of radius R behind the spherical cap of the probe tip penetrating the workpiece in a forward direction was removed. At this time, the removed volume was half of the spherical cap volume and is expressed as follows:

$$V_1 = \frac{1}{2} \pi d_1^2 \left(R - \frac{d_1}{3} \right) \quad (3)$$

where R is the probe tip radius of the cutting tool, and d_1 is the cutting depth during the first cutting pass. CATIA computer-aided design (CAD) software also can be used to establish solid models of the geometric shape in order to calculate removed volume and cutting depth.

In the study, a fixed down force was applied to the workpiece. The radius of the probe tip and the cutting depth were used to calculate the workpiece volume removed during the first cutting pass. CAD software also can be used to simulate and calculate the workpiece volume removed and cutting depth. The SDFE value was obtained by multiplying the down force with the cutting depth and dividing it by the removed volume, as expressed in Equation (2).

4. The SDFE Value of Sapphire Substrate

4.1. The SDFE Value of Sapphire Substrate without Dipping Slurry

Table 2 shows the related AFM experimental data for the first cutting pass of the sapphire substrate without slurry dipping under various levels of down force and at room temperature (23°C). The results in Table 2 were input into the CAD software to calculate the volume removed at that depth. When SDFE equation was input into the calculation, it found that the SDFE values tended to approach the constant value of $0.1827 \mu\text{N}\cdot\text{nm}/\text{nm}^3$.

Table 2. AFM experimental data from the first cutting pass of straight-ling groove cutting of sapphire substrate without dipping in slurry at various levels of down force

down force (μN)	measured cutting depth of the first cutting pass (nm)	removed volume obtained by CAD calculation (nm^3)	removed volume calculated by theoretical equation (nm^3)	SDFE value calculated by theoretical equation ($\mu\text{N}\cdot\text{nm}/\text{nm}^3$)
32.67	0.951	169.71	169.70	0.1828
35.93	1.045	205.24	205.24	0.1827
42.46	1.239	288.37	288.37	0.1826
49.10	1.429	383.39	383.39	0.1827

4.2. The SDFE Value of Sapphire Substrate Dipped in Different Temperatures of Slurry

The experimental parameters were the various dipping temperatures (23°C, 30°C, 40°C and 50°C), the dipping time (60 min), and the volume concentration of the slurry (50%). After dipping the sapphire substrate in slurry with dipping temperature, it applied a small down force for AFM nanoscale cutting of V-shaped groove to obtain the cutting depth and SDFE value of the chemical reaction layer of the slurry-dipped sapphire substrate. Initially, small down force was applied in the nanoscale cutting to ensure that the cutting depth would not exceed the thickness of the chemical reaction layer. Tables 3 and 4 show the results of dipping the sapphire substrate in slurry at temperatures of 23°C and 50°C for dipping time of 60min respectively. An AFM probe tip with radius of 150 nm was used for the experiment. A small down force was applied to cut the sapphire substrate to obtain the value of SDFE_{reaction} of different dipping temperatures of slurry. The term Δd_z denotes the cutting depth and ΔV is the removed volume. Tables 3 and 4 show that when the sapphire substrate was dipped in slurry for 60 min at dipping temperatures of 23°C and 50°C (slurry volume concentration: 50%), the average SDFE value of the chemical reaction layer (i.e., average SDFE_{reaction} value) were 0.1622 $\mu\text{N}\cdot\text{nm}/\text{nm}^3$ (dipping

temperature: 23 °C) and 0.1516 $\mu\text{N}\cdot\text{nm}/\text{nm}^3$ (dipping temperature:50°C), respectively. Using the above mentioned experimental method, this steady also obtained the average values of SDFE reaction of the chemical reaction layer of the sapphire substrate at the dipping slurry temperatures of 30°C and 40°C. They were average SDFE_{reaction} value of 0.1597 $\mu\text{N}\cdot\text{nm}/\text{nm}^3$ (dipping slurry temperature: 30°C) and average SDFE_{reaction} value of 0.1564 $\mu\text{N}\cdot\text{nm}/\text{nm}^3$ (dipping slurry temperature:40°C), respectively.

4.3. Verify the Calculation Cutting Depth by Using Equation of SDFE with the Experimental Result

This study used down force 4.21uN to take an experiment of AFM and obtained the cutting depth of sapphire substrate dipped in slurry for dipping temperature 50°C was 0.118nm. Then, it used equation of SDFE_{reaction} with value of SDFE_{reaction} (0.1516($\mu\text{N}\cdot\text{nm}/\text{nm}^3$)) for dipping temperature 50°C to calculate the cutting depth of sapphire substrate for dipping slurry temperature of 50°C. The obtained calculation cutting depth is 0.1179nm. These two cutting depths are very closed. Therefore, it verifies that the equation of SDFE_{reaction} is acceptable and can be used to calculate the cutting depth of sapphire substrate dipping in different temperatures of slurry.

Table 3. Down force, cutting depth, removed volume, and SDFE_{reaction} value of AFM experiment on a sapphire substrate dipped in slurry for 60 min (slurry volume concentration: 50%; dipping slurry temperature: 23 °C)

down force F_d (μN)	cutting depth Δd_z (nm)	removed volume ΔV (nm^3)	SDFE _{reaction} value ($\mu\text{N}\cdot\text{nm}/\text{nm}^3$)	cutting width (nm)
2.14	0.056	0.7388	0.162207	8.181
2.16	0.057	0.7521	0.162274	8.202
Average SDFE _{reaction} value			0.1622	

Table 4. Down force, cutting depth, removed volume, and SDFE_{reaction} value of AFM experiment on a sapphire substrate dipped in slurry for 60 min (slurry volume concentration: 50%; dipping slurry temperature: 50°C).

down force F_d (μN)	cutting depth Δd_z (nm)	removed volume ΔV (nm^3)	SDFE _{reaction} value ($\mu\text{N}\cdot\text{nm}/\text{nm}^3$)	cutting width (nm)
2.04	0.057	0.7654	0.151621	8.27
2.11	0.059	0.8201	0.151621	8.413
2.21	0.062	0.9056	0.151622	8.625
4.11	0.115	3.1153	0.151621	11.745
Average SDFE _{reaction} value			0.1516	

5. Results

This study obtained experimental data at various dipping temperatures (23°C、30°C、40°C、50°C). The $SDFE_{\text{reaction}}$ values of sapphire substrate for various slurry dipping temperatures obtained from the AFM experimental results and SDFE equation were different. This is because the change of the slurry dipping temperature may change the bonding energy of the chemical reaction layer of sapphire substrate. It also may make sapphire substrate softer and become easy to cut. According to above mentioned experimental results that the $SDFE_{\text{reaction}}$ values for dipping slurry temperatures of 23°C, 30°C, 40°C, 50°C are $0.1622\mu\text{N}\cdot\text{nm}/\text{nm}^3$, $0.1597\mu\text{N}\cdot\text{nm}/\text{nm}^3$, $0.1564\mu\text{N}\cdot\text{nm}/\text{nm}^3$ and $0.1516\mu\text{N}\cdot\text{nm}/\text{nm}^3$, respectively. It can be found that the dipping slurry temperatures increased, the values of $SDFE_{\text{reaction}}$ decreased.

Then, a small constant down force of $3.0\mu\text{N}$ is used to substitute into equation of $SDFE_{\text{reaction}}$ (Equation(2)) to obtain the cutting depths of sapphire substrate for dipping slurry temperatures of 23°C, 30°C, 40°C and 50°C. The cutting depths for dipping slurry temperatures of 23°C, 30°C, 40°C and 50°C obtained by equation of $SDFE_{\text{reaction}}$ are 0.0785nm , 0.0797nm , 0.0814nm , and 0.0840nm , respectively. It can be found that the dipping slurry temperatures increased, the cutting depths increased. These two phenomena concerning the dipping slurry temperatures affected the values of $SDFE_{\text{reaction}}$ and cutting depths can be shown in Fig.1 and Fig.2.

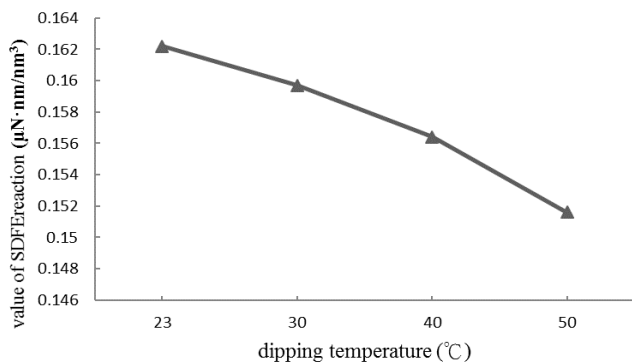


Figure 1. The diagram of tendency between value of $SDFE_{\text{reaction}}$ and dipping temperatures of slurry

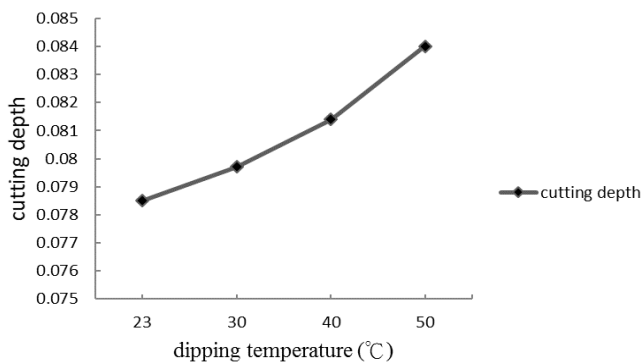


Figure 2. The diagram of tendency between cutting depth and dipping temperature of slurry

6. Conclusions

In optical semiconductor manufacturing processes, chemical mechanical polishing (CMP) is a key technology for the planarization of wafers. Factors influencing the performance of CMP include the composition, volume concentration, and temperature of the slurry, the rotation speed, down force and polishing pad. Thus the temperature of slurry is an important factor affected the performance of CMP. This paper studies the change of specific down force energy and cutting depth of sapphire substrate when sapphire substrates were dipped in different temperatures of slurry. It involved applying small down force in cutting sapphire substrates by atomic force microscope (AFM) before dipping them in slurry in order to obtain the $SDFE$ value of without dipping slurry. Next, small down force was applied to cut sapphire substrates dipped in slurry for varying dipping temperatures to obtain the $SDFE_{\text{reaction}}$ values of dipping slurry with different dipping temperatures. Nanocutting was performed by AFM with a small constant down force to obtain the cutting depths of sapphire substrate for the different dipping temperatures of slurry. The results indicated that the dipping temperature of slurry increased, the $SDFE_{\text{reaction}}$ value of sapphire substrate decreased, and the cutting depth of sapphire substrate with a constant down force increased. This also means that cutting depth of each abrasive particle of CMP will be increased when temperature of slurry increased.

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