

Design and Implementation of a High Power Dual-module Parallel Charging System

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Abstract This paper presents a high-power dual-module parallel charging system which consists of a power converter and digital control software. The power converter consists of an active power factor correction (APFC) circuit and a resonant voltage fed full-bridge converter (RVFFBC). The APFC circuit is used for AC/DC conversion and power factor correction for improved power quality. The RVFFBC is used to provide stable power for charging the battery by converting the high voltage of the power stage to a lower value. The system software was designed by combining the power control loop into a voltage and current loop to achieve current sharing of the dual-module charging system and to overcome the effect of differences in hardware components. Finally, this paper demonstrates the implementation of a high-power dual-module charging system with a widely varying AC input voltage ranging from 85 ~ 265 Vac. Experimental results verified that the maximum power factor of the system and the Total Harmonic Distortion (THD) were 0.99 and 2.8% respectively. The proposed charging system possesses very high expansibility. The parallel dual-module output DC current of the system is 70 A and the total output power is 4 kW.

Keywords Active Power Factor Correction, Full-Bridge Converter, Parallel Charging System, THD

1. Introduction

With the increase in the use of devices such as laptops, mobile phones, tablet PCs, etc., lithium batteries have gradually replaced lead-acid batteries as the power source of choice. Similarly, with the increase in the demand of battery capacity for use in applications such as electric vehicles (EV) and uninterruptible power systems (UPS), the characteristics of the charging systems of these batteries have assumed great importance [1]-[4], with a great deal of work being carried out in this area. The desired features of a good charging system are an improved power factor and low harmonic pollution.

Traditional AC-DC converters consist of a bridge rectifier and a filter capacitor. The advantages of such converters are

simplicity of the circuit structure and ease of control. However, they exhibit serious nonlinear distortion, which not only causes the power factor to be reduced, but also affects the device and power network equipment. It also affects the quality of the overall electrical supply system. This leads to poor power grid stability and power loss. Therefore, a power factor correction (PFC) circuit is generally used to improve these problems. The PFC circuit can be divided into two: active power factor correction (APFC) circuits and passive power factor correction (PPFC) circuits [5]-[7]. The correction capability of PPFC circuits is low and they are unable to meet standard requirements. APFC circuits use the Pulse Width Modulation (PWM) scheme, which leads to the input current and voltage waveforms having approximately the same phase. APFC circuits therefore meet the standard requirements and specifications. Current APFC circuits can achieve power factors in the range of 0.98~1, which enhances the power conversion efficiency and power quality of high-power high-current charging systems.

Typical charging systems which provide stable power source is designed by DC/DC converter circuit, it convert a high DC voltage to a low DC voltage in order to match the voltage of the battery pack. Commonly-used step-down DC/DC converter circuits such as buck, buck-boost, etc., suffer from the inherent disadvantages of having large current ripples and low output powers. To overcome these deficiencies, a full bridge converter circuit with a center tap rectifier filter circuit is proposed in this paper. Such a circuit has a highly stable output voltage and current.

In general, to improve the system's expansibility and usability, the charging system consists of several modules to increase the output power [8]-[13], [19]-[22]. The key point of multi-module parallel operation is current-sharing. If the output current is not shared equally among modules, it will result in one module getting easily damaged, which can lead to system shutdown. Poor current sharing and complicated control are the main drawbacks of traditional parallel charging systems. Therefore a dual-module high power charging system in parallel operation that exhibits better current-sharing and control properties is presented in this paper.

2. Charging System Architecture

Fig. 1 shows the proposed single module charging system architecture. It can be divided into three parts. The first is the APFC circuit [14],[15] which is used to improve the power quality. The second is the RVFFBC which is used to provide stable power for charging the power battery. The third is a rectifier filter circuit with a center tap [16]-[18]. The PWM signal is generated by the microcontroller and the D/A converter circuit is used to convert the MCU signals to control the output current of the UC3846 IC. Each part will be illustrated in the following sub-sections.

2.1. Active Power Factor Correction (APFC)

A commonly-used PFC circuit architecture includes a buck, buck-boost, boost, SEPIC converters, etc. Table 1 gives a comparison of the features of various converters. To meet the specifications of the proposed single module charging system, the Boost converter was used, as shown in Fig. 2. The IC L4981 was used to control the boost converter to achieve a power factor of about 0.99 with a widely varying AC input voltage (85Vac-265 Vac). The PFC circuit can operate in the continuous conduction mode (CCM) and can be used in charging systems of up to 500 W.

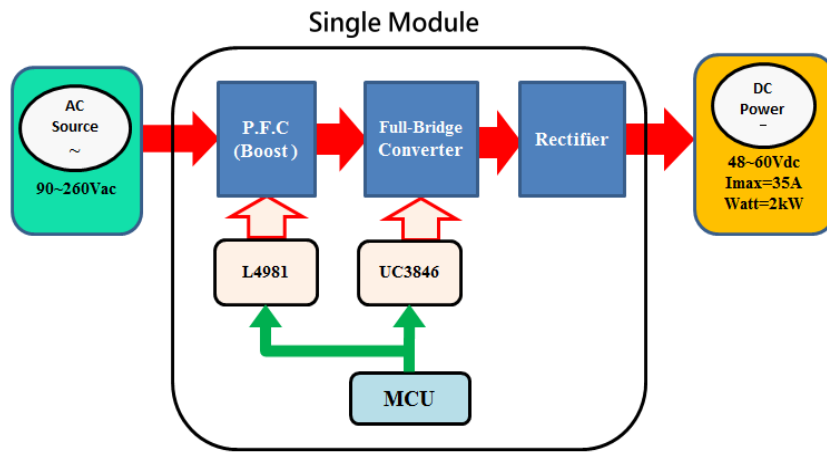


Figure 1. Single module charging system architecture.

Table 1. A comparison of the features of various converters.

	Buck	Boost	Buck-Boost	SEPIC
V_o Polarity	Positive	Positive	Negative	Positive
Crossover Distortion	Yes	No	No	No
Number of components	Less	Less	Less	More
PFC	Low	Highest	Low	High

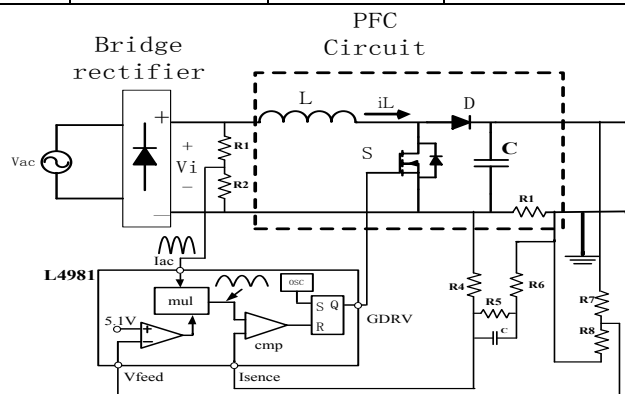


Figure 2. Architecture of APFC.

2.2. Resonant Voltage Fed Full Bridge Converter (RVFFBC)

The architecture of the RVFFBC is shown in Fig. 3. The resonance is generated by the resonant transformer, the inductor L_r , and the parasitic capacitor of the power switches. Thus, zero voltage switching (ZVS) of the power switches is achieved as shown in Fig. 4. It also greatly improves the overall efficiency and stability of the system and reduces Electro-Magnetic Interference (EMI).

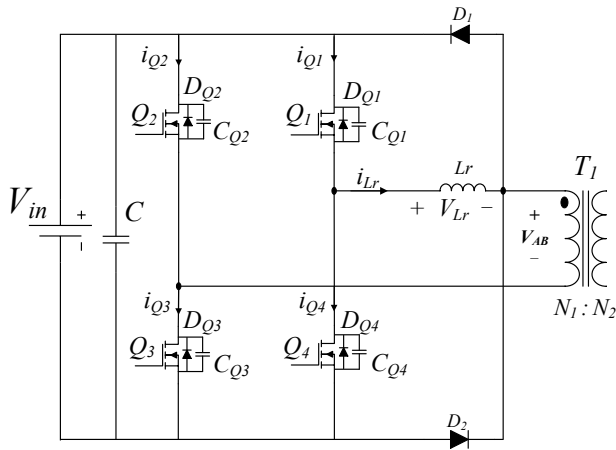


Figure 3. Architecture of RVFFBC.

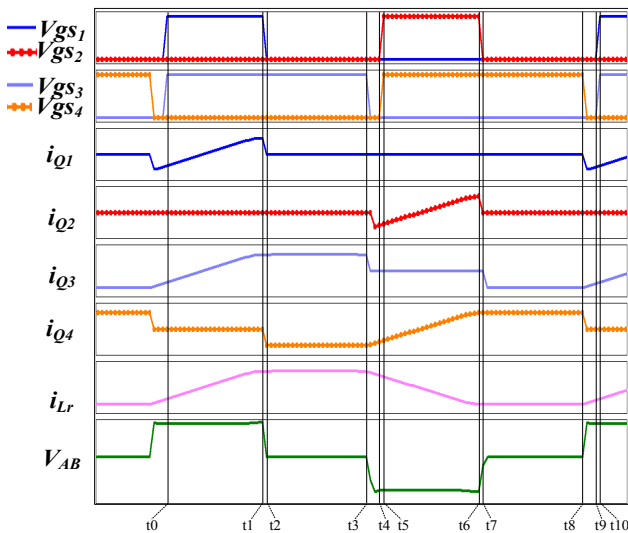


Figure 4. Key waveforms of RVFFBC.

The operation of the RVFFBC is divided into positive and negative half-cycles. As the operation is similar in each half-cycle, only the positive half-cycle is described in this paper. The positive half-cycle operation mode is divided into five intervals $t_0 - t_5$ as shown in Fig. 5. The operation first enters the energy clamping stage, and then enters the Mode 1 ~ Mode 5 interval operation, it is illustrated as follows.

Energy clamping interval

This interval is shown in Fig. 5(a), which is used to improve the energy imbalance between the resonant inductor and the transformer. Clamping diodes D_1 and D_2 improve the oscillation generated by the reverse recovery time of the rectifier diode and stabilizes the unstable energy state between the transformer and the resonant inductor L_r .

Mode 1: Energy transfer interval [t_0-t_1]

The switches Q_1 and Q_3 are turned on as shown in Fig. 5(b). V_{in} is equal to the sum of the inductor voltage V_{Lr} and the transformer's primary voltage V_{AB} . The input current flows from switch Q_1 to Q_3 and energy is transferred to the transformer and the resonant inductor L_r .

Mode 2: Resonant state interval [t_1-t_2]

The switch Q_3 is kept in the on-state and Q_1 is turned off, as shown in Fig. 5(c). The current direction is the same as in Mode 1. The parasitic capacitor C_{Q1} of Q_1 is charged and the parasitic capacitor C_{Q4} of Q_4 is discharged. Therefore, the voltage across Q_4 is reduced.

Mode 3: Energy hold interval [t_2-t_3]

The inductor L_r releases energy and the switch Q_3 is kept in the on state, as shown in Fig. (d). After the discharge of C_{Q4} to turn on D_{Q4} , the voltage across Q_4 is reduced. Thus, Q_4 is turned on under ZVS.

Mode 4: Resonant state interval [t_3-t_4]

The switch Q_4 is kept in the on-state, as shown in Fig. 5(e). The resonant effect is generated by the resonant inductor and the parasitic capacitor of C_{Q3} and C_{Q2} . The switch Q_2 is turned on under ZVS at this moment.

Mode 5: Energy transfer interval [t_4-t_5]

The switches Q_2 and Q_4 achieve ZVS under the resonant effect, and the current flow direction is from Q_2 to Q_4 . The positive half cycle operation is over and the device enters the negative half-cycle at this time, as shown in Fig. 5(f).

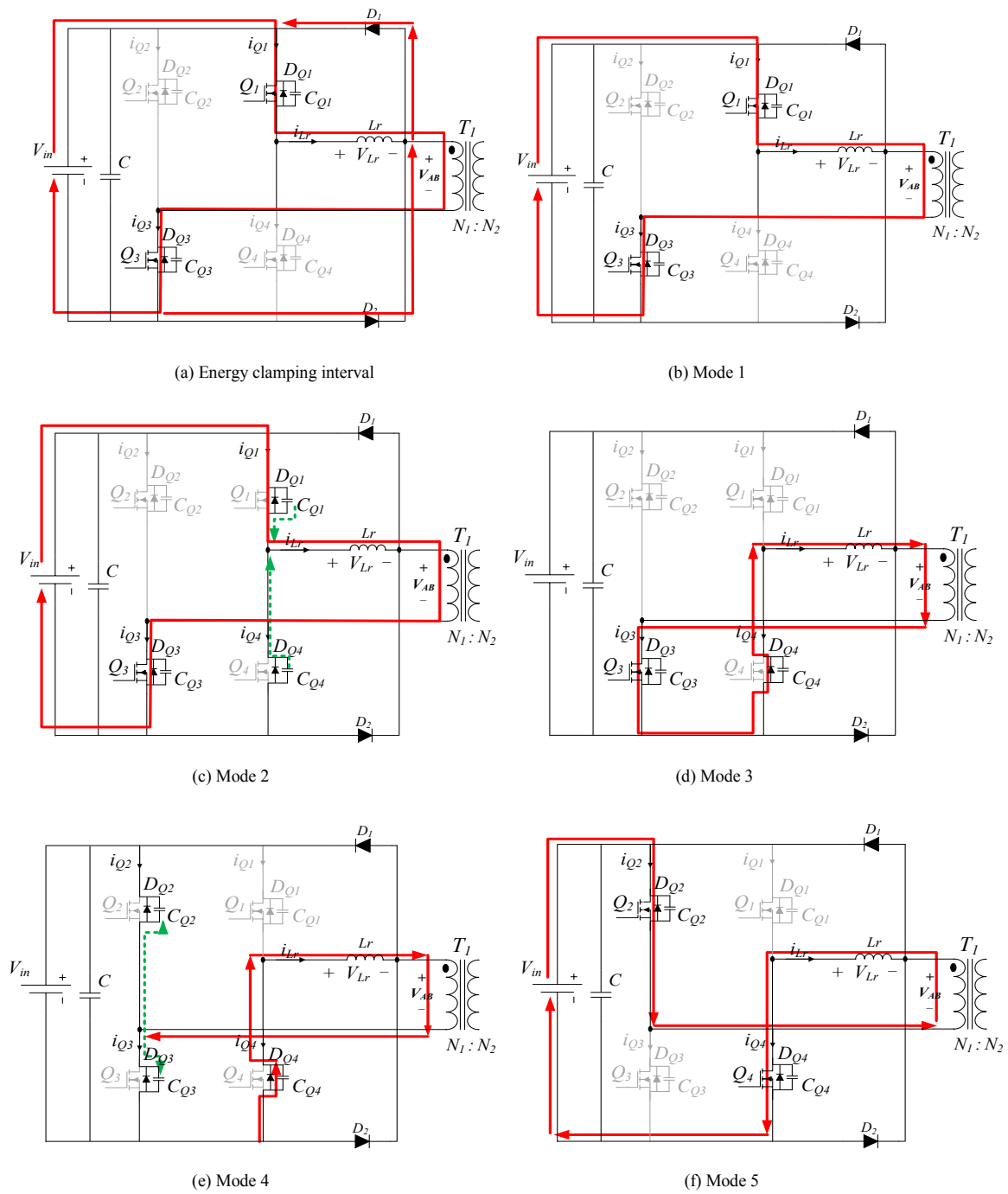


Figure 5. RVFFBC operating mode under the positive half cycle.

2.3. Rectifier Filter Circuit

Fig. 6 shows the rectifier and filter circuit with the center tap transformer double winding, which provides the positive and negative half-cycles. Therefore, the output current ripple has a frequency which is twice that of the switching frequency of the power switches. This results in a stable DC output voltage and a small current ripple.

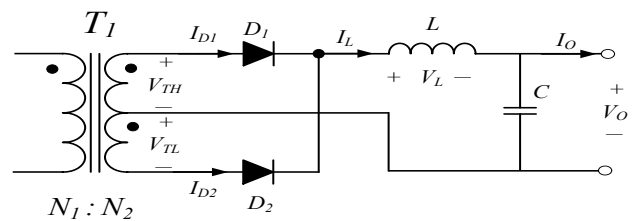


Figure 6. Rectifier and filter circuit.

2.4. Parallel Operation of Dual-module Charging System

The proposed architecture of the dual-module charging system is shown in Fig. 7. To achieve current sharing, the master microcontroller outputs a reference current to adjust the output of the other module. Thus, the parallel operation dual module charging system is implemented by the current sharing scheme, and its control block is shown in Fig. 8. The

outer loop is the feedback voltage V_{bat} that regulates the output voltage and the inner loop is the feedback current I_{out} that improves the dynamic response. In addition, the output power loop, which is generated by the product of the feedback voltage and current, is used to establish the common reference power P_{ref} for achieving the same output power of each module. Fig. 8 shows the hardware of the dual-module charging system.

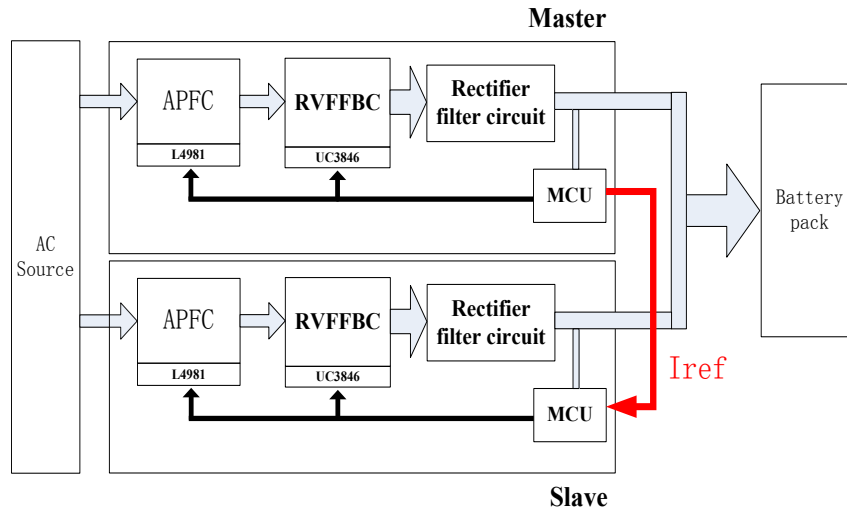


Figure 7. Dual-module charging system architecture.

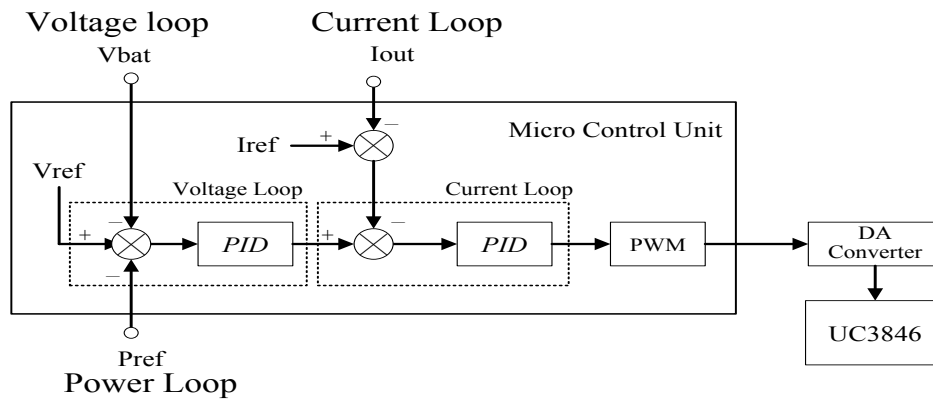


Figure 8. Control block diagram of the dual-module charging system.

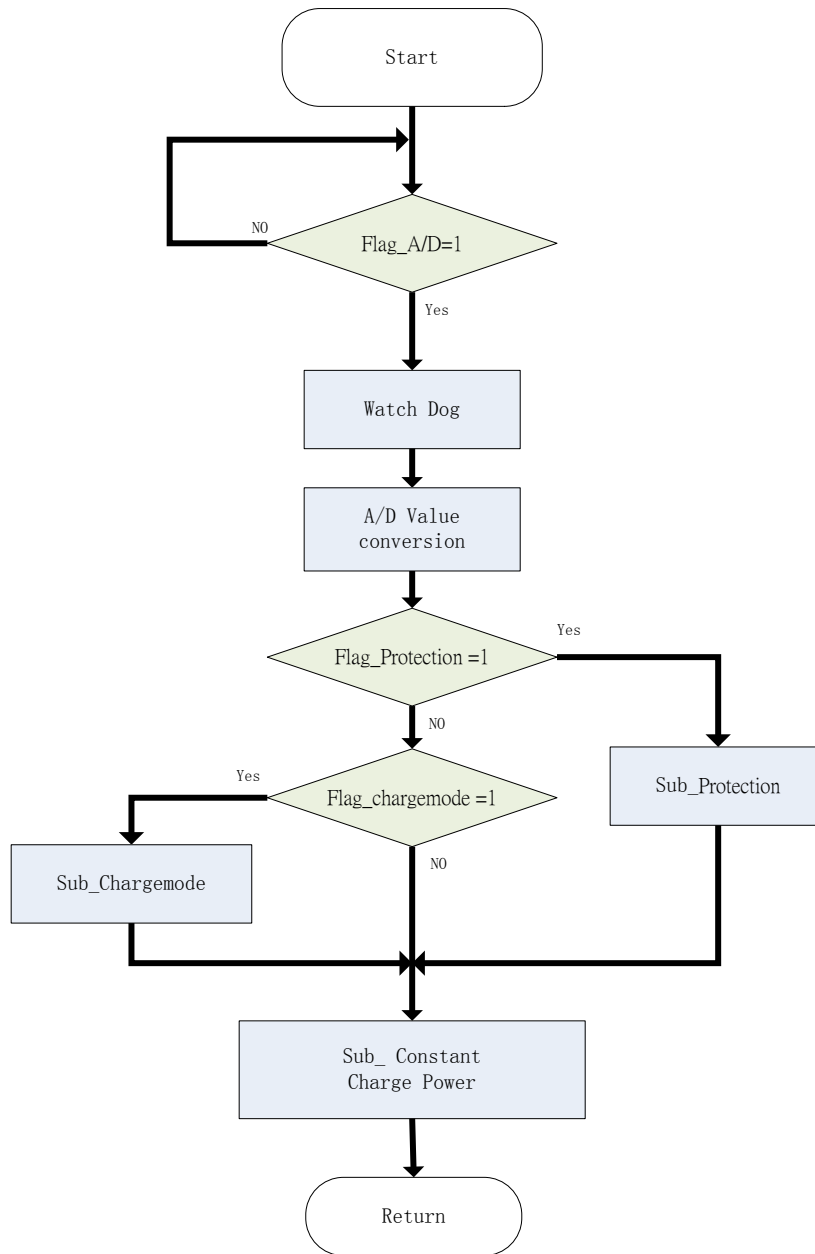


Figure 9. System program flowchart.

3. System Program

Fig. 9 shows a system program flowchart which contains the following three subroutines: the charge mode program, the protection program, and the constant charge power program. These are explained as follows.

3.1. Charge Mode Program

Table 2 shows the charging/discharging specification of the battery cell. It can be seen that the charging method of the battery cell is constant voltage-constant current (CV-CC), and the battery cell’s maximum charging current and voltage were 3 A and 3.65 V, respectively. The charging voltage of the charging system must be determined according to the battery cell’s charging curve, as shown in

Fig. 10. Therefore, 16 battery cells were connected in series to constitute a battery pack whose maximum charging voltage was 58.4 V.

Table 2. The charging/discharging specification of the battery cell.

Operation Conditions		
Charging Voltage	3.65 V	
Charging Method	CC-CV	
Cut-off Discharge Voltage	2.10 V	
Max. Continuous Discharge Current	10 A	
Max. Charge Current	3 A	
Operating Temperature Range	Discharge	-10 ~ 55 °C
	Charge	~ 45 °C

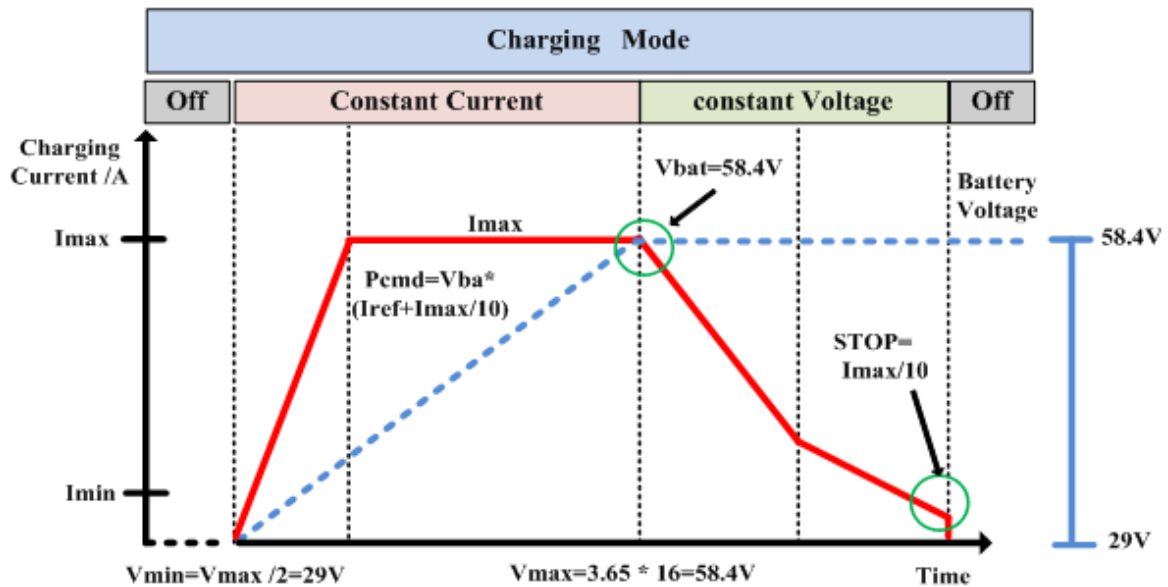


Figure 10. Charging curve of the charging system.

The charging procedure consists of three steps which are explained below.

1. Battery Low Voltage Detection

Fig. 11 shows a flowchart of the charging mode program. First, it is determined whether the battery voltage is $> 29V$. If it is, then the battery may be damaged or the wiring may be abnormal. The output power command (P_{cmd}) must be set to low. If the battery voltage is $< 29V$, it represents that the battery can be charged properly.

2. Constant Current: CC

The initial value of the output current is 0, and considering the battery capacity, the output power command (P_{cmd}) which according to the 1/10 setting value of maximum current (I_{max}) gradually increase, it can ensure the output current of different battery capacity sets the value of the maximum current to 1/10 of its value to ensure that

the output current matches the capacity of a different battery. When the output power command (P_{cmd}) increases to the maximum current (I_{max}), the charging system output current (I_{ref}) corresponds to the maximum output current command (I_{max}). This value is maintained until the battery voltage reaches 58.4 V. Then, the charging mode changes.

3. Constant Voltage: CV

When the battery reaches the maximum voltage (V_{max}), it represents the battery as being under pseudo saturation. In order to charge the battery to saturation, 1/10 of I_{max} is taken as the charging system shutdown command. It must be ensured that the battery voltage does not exceed V_{max} . While the battery current gradually decreases and the battery voltage gradually stabilizes, the charging system will immediately shut down when the charge current is less than 1/10 of I_{max} .

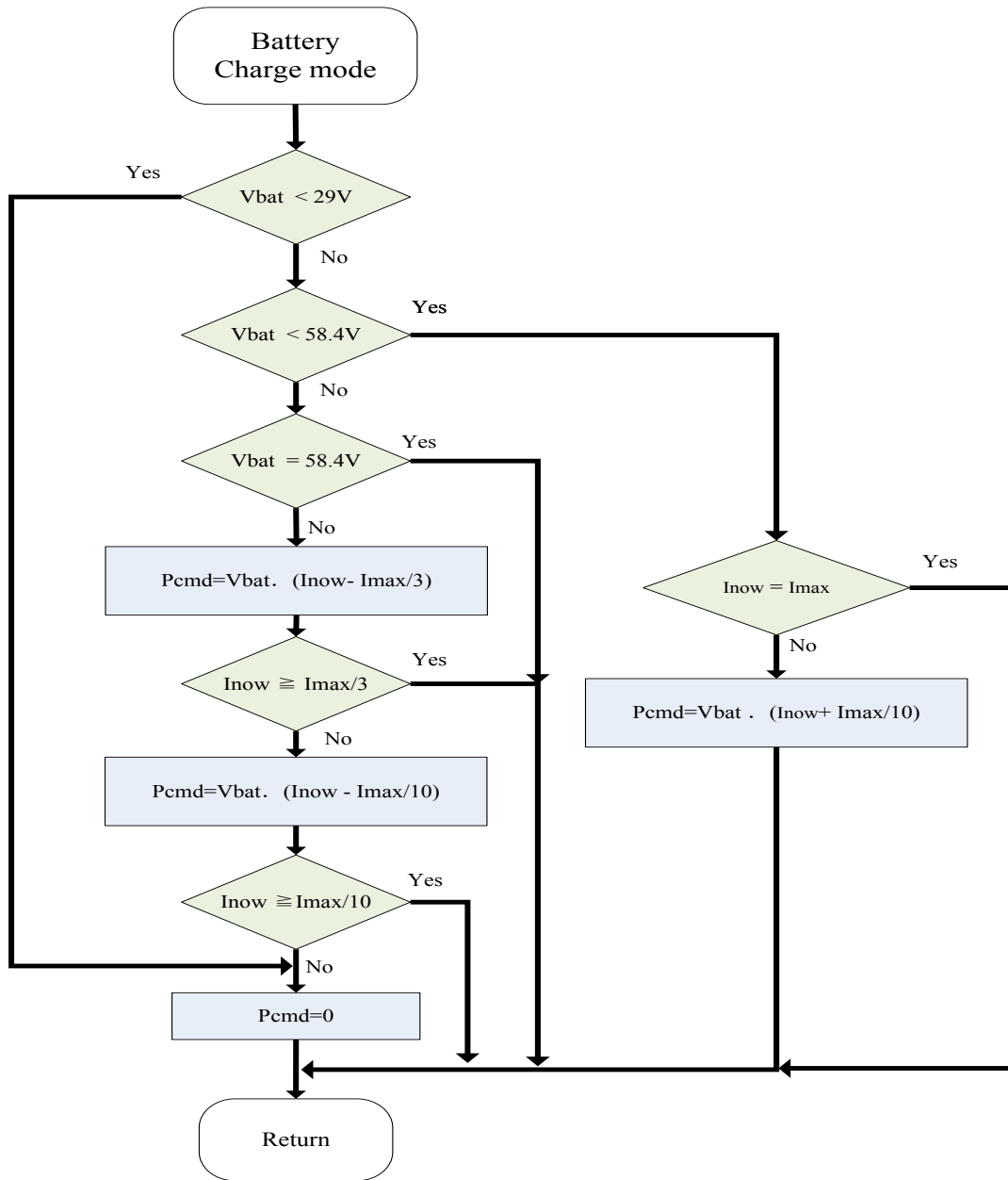


Figure 11. Charging mode program flowchart.

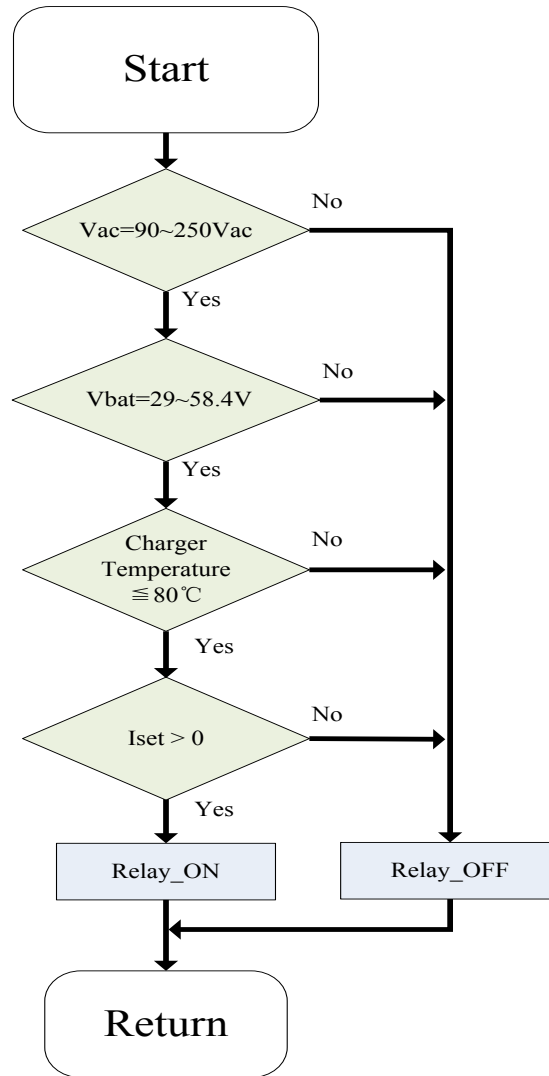


Figure 12. Protection program flowchart.

3.2. Protection Program

Fig. 12 shows a flowchart of the protection program. It can be seen that the protection items of the charging system include input voltage, battery voltage, charger temperature, and charge current.

3.3. Constant Charge Power Program

Constant power control possesses the function of limiting the maximum value of the system power; its output control is to change the rating of the current regulator. Such a control scheme can achieve a fast response of the DC current regulation loop. In addition, it can also substantially prevent transients and fluctuations generated by the severe variation of the feedback circuit.

Fig. 13 shows a flowchart of the constant charge power program which consists of three protection functions. First, consider the security protection. When the instantaneous output exception occurs, that is, when the product of battery

voltage V_{bat} and output current I_{out} is greater than the constant power, it must be immediately determined whether the battery voltage is $> 58.4V$ or $< 29V$. If it does, the output power command P_{cmd} is immediately set to 0. This avoids charging the system by overcurrent caused by a short circuit.

The maximum temperature protection is called the drop power function. We must detect whether the current temperature T_{now} reaches the over-temperature; the temperature must reach $70^{\circ}C$ before entering the computing equation, and the maximum temperature T_{max} is designed to be $80^{\circ}C$; if it does, it means that the temperature of the charging system is higher than $70^{\circ}C$. The charging system is turned off when the temperature reaches $80^{\circ}C$.

Finally, the last function of the constant charge power program is overload protection. To calculate the current battery voltage V_{bat} and the maximum current I_{max} , if the output power of the charging system is greater than the maximum power, then maximum power output is maintained. This approach can limit the maximum output power of the charging system and avoid overload and damage.

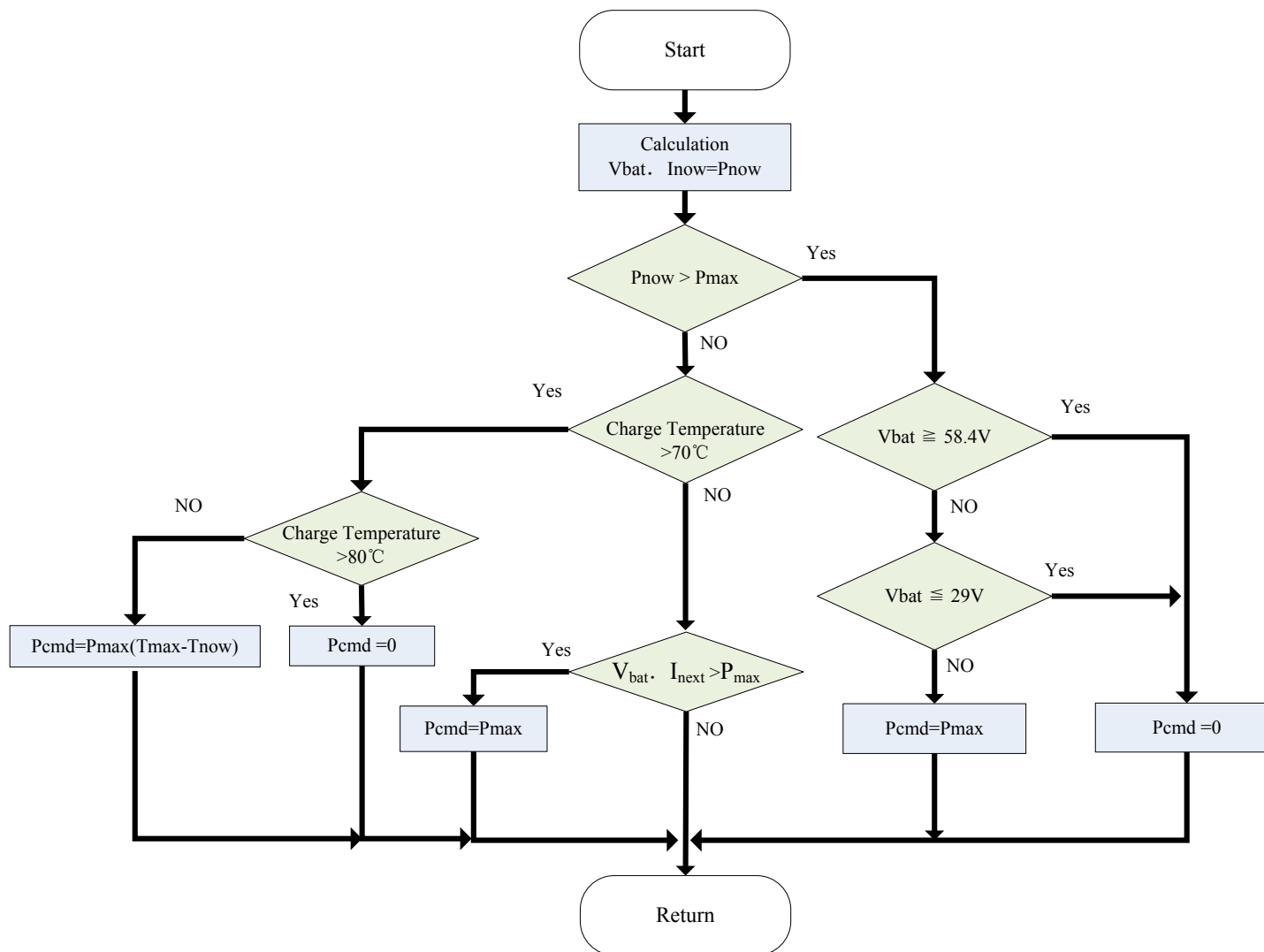


Figure 13. A flowchart of the constant charge power program.

4. Experimental Results and Discussions

Table 3. System components and electrical specifications.

	Boost	RVFFBC
L / Lr	0.53 mH	10 uH
Diode	DSEP30-06B	Mur3020pt
MOSFET	24N60C3	P25NM50N
	Single-module	Dual-module
Input Voltage	90-260 Vac	90-260 Vac
Output Voltage	48-60 Vdc	48-60 Vdc
Max. Current	35 A	70 A
Output Wattage	2 kW	4 kW

In this paper, a dual-module charging system using a parallel architecture with a digital microcontroller

P89LPC938 is implemented. Its maximum output current is 70 A and the output power is 4 kW. Table 3 shows the system’s electrical specifications and component specifications.

4.1. Single Module Verification

This section starts by testing the effectiveness of a single-module. Fig. 14(a)–(d) shows the input and output measured waveforms operating under a light load and a full load, respectively. The light load input power was 336.7 W and the output power was 290.1 W. The full load input power was 2096.2 W and the output power was 1904 W. Fig. 15 shows the efficiency curve of the single module under different operating powers. It can be seen that the highest efficiency was 89.7% and the full load efficiency was 89%.

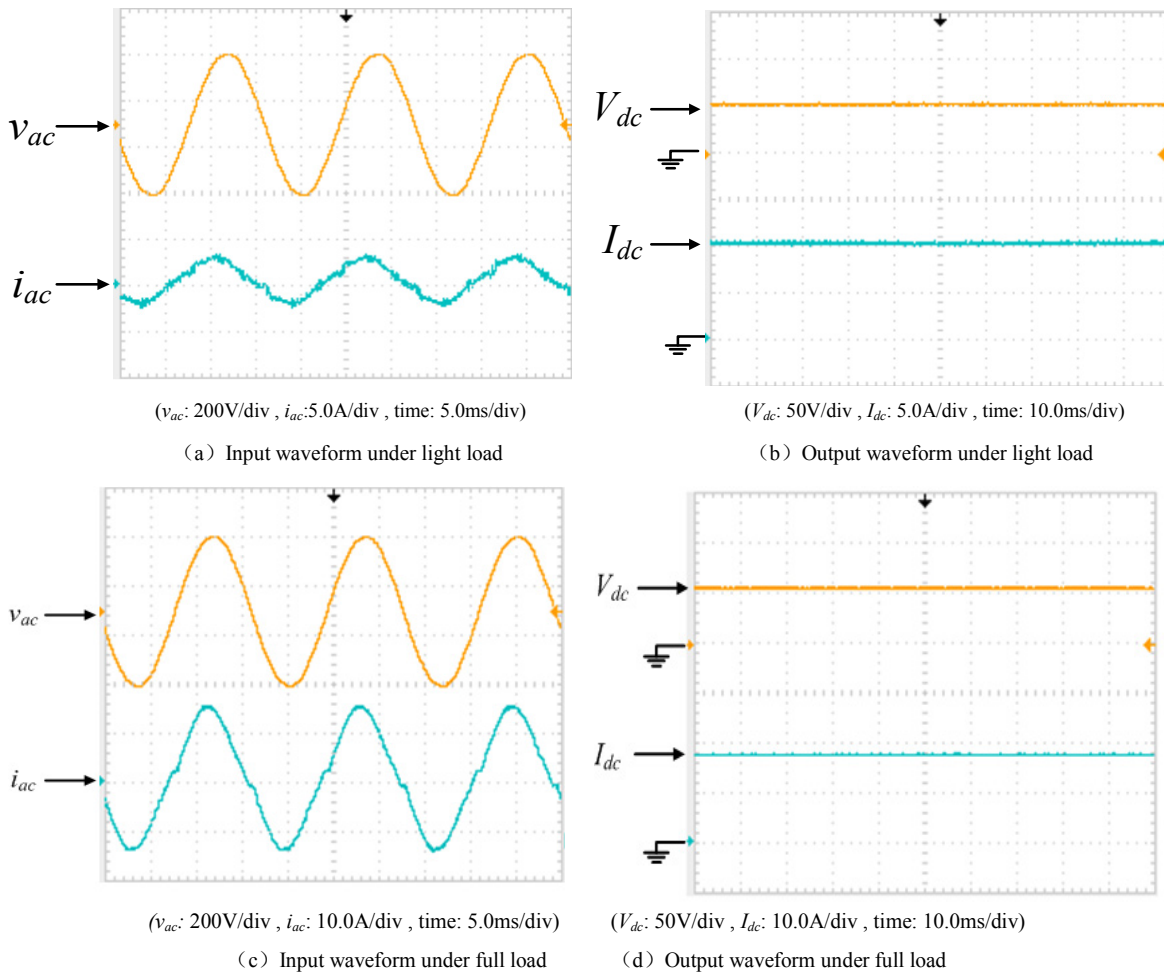


Figure 14. Input/output waveforms of single module.

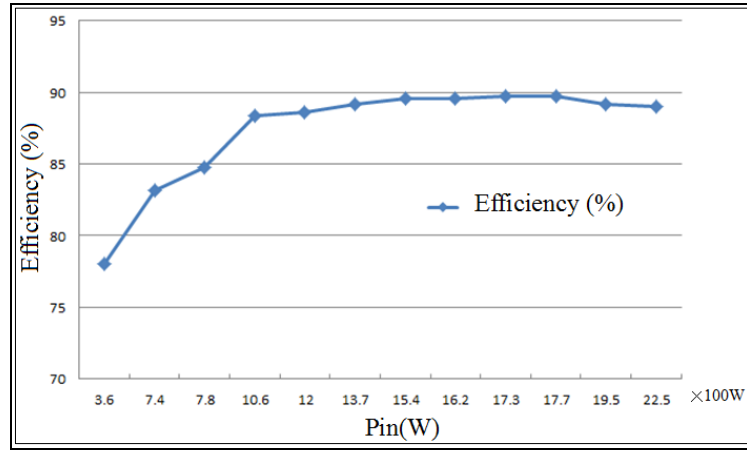
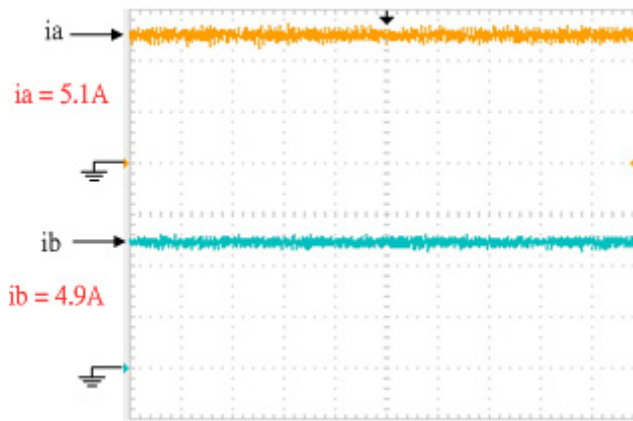


Figure 15. Efficiency curve of a single module.

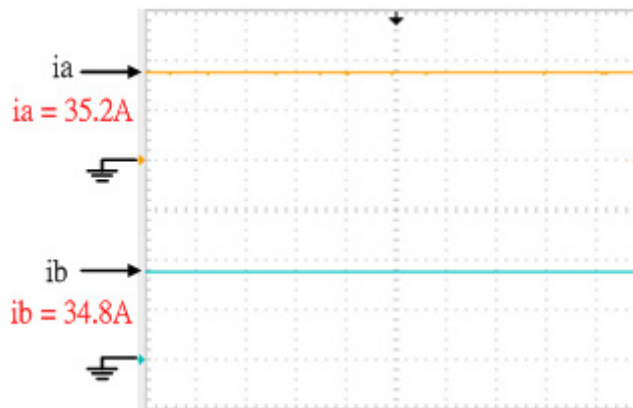
4.2. Current Sharing of Dual-Module Measurement

Fig. 16 shows that the total output current under light load was 10 A and that the current error was 0.2 A. Fig. 17 shows that the total output current under full load was 70 A, and that the current error was 0.4 A. Fig. 18 shows the current error comparison of the dual-module under different operating powers. It can be seen that the proposed dual module charging system exhibits good current sharing behavior.



(Ia: 2.0A/div ; Ib: 2.0A/div ; time: 10.0ms/div)

Figure 16. Measured output current of dual module under light load (10 A).



(Ia: 20.0A/div ; Ib: 20.0A/div ; time: 10.0ms/div)

Figure 17. Measured output current of dual module under full load (70 A).

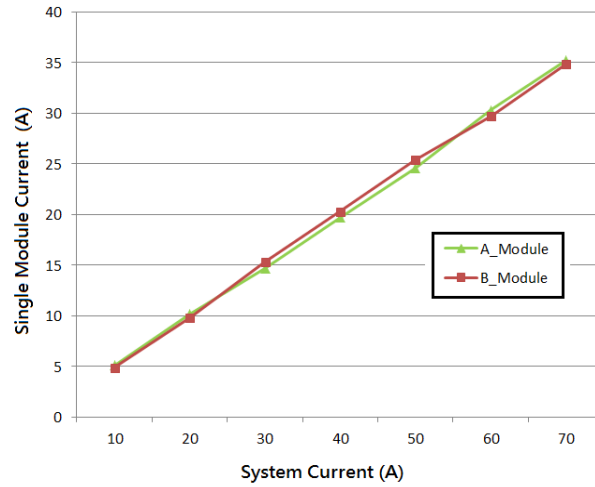
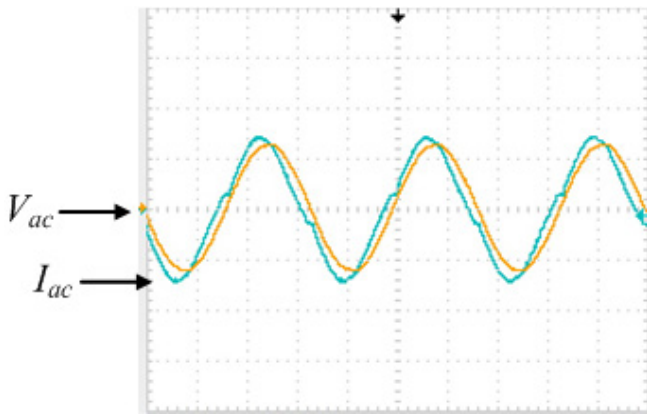
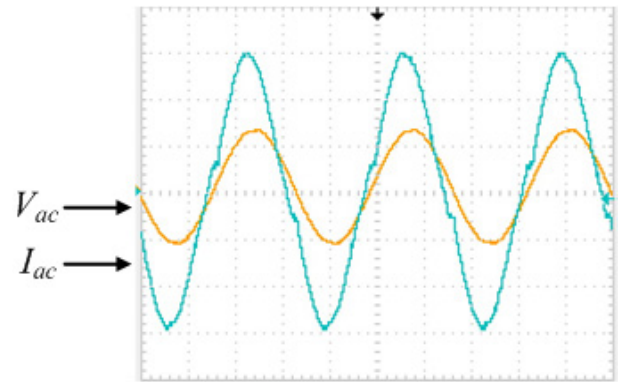


Figure 18. Current error comparison of dual module charging system.



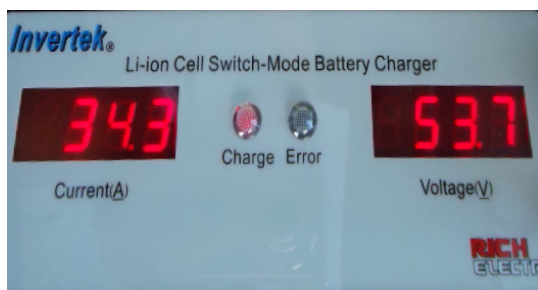
(vac:250V/div ; iac:10.0A/div ; time:5.0ms/div)

(a) Input voltage and current



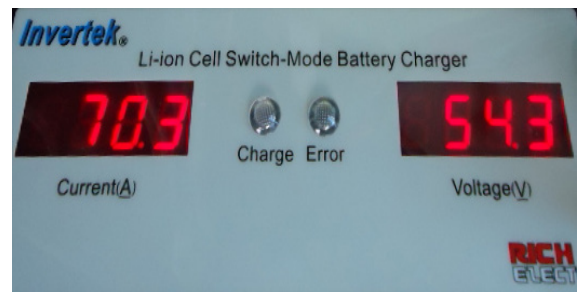
(vac:250V/div ; iac:10.0A/div ; time:5.0ms/div)

(a) Input voltage and current



(b) Output voltage and current

Figure 19. The input/output voltage and current of a single module.



(b) Output voltage and current

Figure 20. The input/output voltage and current of a dual module.

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