Simulation of Comparison from NRZ and RZ Pulse in Free Space Optics with Different Weather Conditions

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Abstract FSO (Free Space Optic) is a form of optical technology communication by transmitting light to media free space. In the FSO system, the data transmission can be larger, namely 1-100 Gbps, and this is due to the large bandwidth width. FSO runs at a wavelength of 850 nm and 1550 nm. FSO is usually with a maximum distance of 2-4 km. This paper simulates the FSO optical transmission system using NRZ and RZ line coding in bright and rainy weather conditions. The parameters analyzed are Eye diagram, Optical Spec-trum, photocurrent, and received signal power. In the FSO line coding system, NRZ has an eye height value, received signal power and received photocurrent is greater than the RZ line coding at a distance of 1 km and 5 km in bright and rainy conditions. In the trial of this FSO communication system, it is better to use it at a distance of 1 km, because the received signal power is above 20 dBm and received photocurrent is still above 800 mA for NRZ and RZ line coding. This is due to the attenuation value of sunny weather conditions that are smaller between 0.2-3 dB/km, while in rain conditions between 4-17 dB/km.

Keywords FSO, Eye Diagram, Signal Power, Photocurrent, Optical Spectrum

1. Introduction

FSO (Free Space Optics) is an optical communication technology in which data is transmitted by light propagation in empty space that allows optical connectivity. The FSO works almost similar to the OFC (Optical Fiber Optics) network but the only difference is that the FSO is sent by free air while the OFC is sent using glass fiber using cables. FSO communication offers a wide bandwidth potential that can provide high data rates [17]. Making this type of communication system is very interesting in meeting the consumers' large demand supported by high internet.

FSO is an environmentally friendly communication system because it has low price, high-speed data transmission and is easy licensed in the building window. Using an FSO can send data over 1-100 Gbps due to the large bandwidth width. FSO runs at a wavelength of 850 nm and 1550 nm [16]. FSO data links can be fully integrated into current short and longhaul high speed optical networks. Utilizing current 1550 nm technology platforms FSO data links can fully attain current system architectures, additionally the systems can be completely scaled to higher data rates and configurations. So that the FSO system provides comfort to the user [18]. FSO is usually with a maximum distance of 2-4 km.

There are several shortcomings of the FSO (Free Space Optics) communication system in poor weather conditions, which will affect the work of the FSO, like in obstruction of rain, fog, and dew. In addition to weather factors, there are also technical factors, like the lack of precision in the installation of light between FSO, blocked by escalators.

2. Theoretical Foundation

2.1. FSO Communication System (Free Space Optics)

The FSO communication system (Free Space Optics) or often referred to as optical wireless, is an optical communication system that uses the atmosphere as its propagation media. The FSO uses light beams to send full-duplex Gigabit Ethernet data, voice and video communication throughput through air intermediaries. The light source used can be either LED (Light Emitting Diode) or Laser (Light Amplification by Stimulated Emission of Radiation) [1]. The sending is binary data with NRZ, AMI, NRZ-L and so on. Usually FSO is used between buildings such as point-to-point, mesh, point-to-multipoint and ring. The FSO topology image is presented in Figure 1 below.

Figure 1. FSO Network System [2]

Figure 2. FSO Communication Work System [3]

2.2. FSO Communication Work System

In the FSO communication work system, network traffic becomes pulses that have binary numbers, namely numbers 1 and 0. After that, the transmitter works to send data through an air intermediary with light. Then, the receiver will receive data from the transmitter via the photodetector. In the end, the signal obtained from the receiver will be connected to fiber or copper connected to the network.

For the formula at [13]:

$$P_{\text{Received}} = P_{\text{Transmitted}} \frac{d_R^2}{(d_T + \theta R)^2} 10^{-\alpha \frac{R}{10}} \quad (1)$$

Where: d_R = Receiver aperture diameter (m)

d_T = Transmitter aperture diameter (m)

θ = Beam divergence (mrad)

R = Range (km)

α = Atmospheric attenuation (dB/km)

2.3. Damping Concept on Geometry

In the concept of geometric attenuation caused by deviations from beam optic transmission between the transmitter and receiver with the following equation [7]:

$$L_{\text{geo}}(\text{dB}) = 10 \log \left(\frac{d_2}{d_1 + 100L\theta} \right)^2 \quad (2)$$

With L_{geo} is geometric attenuation (dB), d_1 and d_2 are optical transmitters and receivers (cm), L is the distance between sender and receiver (km), and θ is the angle of divergence (mrad) [8].

2.4. Signal to Noise Ratio (SNR)

Noise in the FSO system can be divided into two parts, namely thermal noise and shot noise. The SNR value on the FSO system is as follows [9]:

$$\text{SNR}_{\text{FSO}} = \frac{(\mathfrak{R}P_R)^2}{2q i_S B + 4kTB/R_L} \quad (3)$$

$\mathfrak{R}$ is the recipient's responsiveness at $\lambda = 1550$ nm, q is the large electron charge (C), B is the bandwidth (Hz), i_S the received signal current (mA), k is the Boltzman constant (J/K), T is the temperature (K) and R_L is load resistance (Ω) [8].

2.5. Bit Error Rate

The FSO system BER parameter Algorithm defines the numerical method to use for the BER estimation. Assuming Gaussian noise with the standard deviations σ_0 and σ_1 , the BER is [12]:

$$P_e = \frac{M}{N+M} P_{e0} + \frac{N}{M+N} P_{e1} \quad (4)$$

Where P_0 and P_1 are the probabilities of the symbols, M is the number of samples for the logical 0, and N is the number of samples for the logical 1. Also, P_{e0} and P_{e1} are:

$$P_{e0} = \frac{1}{2} \operatorname{erfc} \left(\frac{S - \mu_0}{\sqrt{2}\sigma_0} \right) \quad (5)$$

$$P_{e1} = \frac{1}{2} \operatorname{erfc} \left(\frac{\mu_1 - S}{\sqrt{2}\sigma_1} \right) \quad (6)$$

Where μ_0 , μ_1 , σ_0 and σ_1 are average values and standard deviations of the sampled values respectively, and S is the threshold value.

An enhancement of the simple Gaussian approximation can be achieved by averaging the separately estimated BERs for different sampled symbols [14]. For M sampled values for the logical 0 and N sampled values for the logical 1, the corresponding error rates are:

$$P_{e1} = \frac{1}{2N} \sum_{i=1}^N \operatorname{erfc} \left(\frac{\mu_{1i} - S}{\sqrt{2}\sigma_{1i}} \right) \quad (7)$$

$$P_{e0} = \frac{1}{2M} \sum_{i=1}^M \operatorname{erfc} \left(\frac{\mu_{0i} - S}{\sqrt{2}\sigma_{0i}} \right) \quad (8)$$

The eye height is calculated by [15]

$$E_H = (u_1 - 3\sigma_1) - (u_0 + 3\sigma_0) \quad (9)$$

2.6. Receiver Power

In the equation to calculate the receiving power as follows [10]:

$$P_r = P_t L_{atm} L_a X + n_{FSO}(t) \quad (10)$$

At L_{atm} is atmospheric losses which include loss of weather and scintillation losses (L_{sint}), while L_a includes geometric losses (L_{Geo}), and system losses (L_{system}), X are variations in signal fading un-der turbulence conditions with probability of fluctuating indices bias, $n_{FSO}(t)$ is the characteristic of AWGN (Additive white Gaussian noise), and P_t and P_r are calculated in mW [8]. After that, it can only calculate the signal power (dBm).

2.7. NRZ and RZ Pulse

In telecommunication, NRZ and RZ systems pulse is a type of line coding. Line coding is a process of converting digital data into digital signals, assuming that data contains or takes the form of faxes, numbers, images, audio, or video stored in computer memory as bit sequences [10]. In non-return to zero (NRZ) modulation is a binary code that is represented by one significant condition, usually a positive voltage, while zero is represented by a negative voltage. Pulses on NRZ have more energy than return to zero (RZ). While modulation of return to zero (RZ) describes line code used where at the time the signal drops to zero between each pulse in the telecommunications signal. This will occur even if 0 or 1 consecutive numbers occur in the converted signal [4].

The NRZ Pulse component produces rectangular non-return to zero (NRZ) electrical pulses with the

following edge shapes is exponential [5]:

$$E(t) = \begin{cases} 1 - e^{-\left(\frac{t}{c_r}\right)}, & 0 \leq t \leq t_1 \\ 1, & t_1 \leq t < t_2 \\ e^{-\left(\frac{t}{c_f}\right)}, & t_2 \leq t < T \end{cases} \quad (11)$$

And the RZ Pulse component produces rectangular return to zero (RZ) electrical pulses with the following edge shapes is exponential [5]:

$$E(t) = \begin{cases} 1 - e^{-\left(\frac{t}{c_r}\right)}, & 0 \leq t \leq t_1 \\ 1, & t_1 \leq t < t_2 \\ e^{-\left(\frac{t}{c_f}\right)}, & t_2 \leq t < t_c \\ 0, & t_c \leq t < T \end{cases} \quad (12)$$

2.8. Different Weather Conditions

The bad weather conditions will affect the performance of the communication system of the FSO, such as sunny, rainy, snowy, thin fog and thick weather. The following is the weakening distance of the FSO communication system, namely:

Table 1. Attenuation with Different Weather Conditions [6]

Condition	Attenuation
Bright	0.2-3 dB/km
Rain	4-17 dB/km
Snow	20-30 dB/km
Luminous Mist	40-17 dB/km
Thick fog	80-200 dB/km

Figure 3. FSO System Design Flow Chart

2.9. Free Space Optics System Design

In figure 3, it can be seen that the information signal is converted into a digital signal on the NRZ and RZ coding line, and then the signal is forwarded to the Mach Zender modulator to convert digital signals converted to light and sent. The receiver is the receiver of the data signal and converts it to the data signal, and then the signal will be filtered on the low pass bessell filter and read by BER

analyzer (Bit Error Rate Analyzer), then the eye diagram will be obtained in this simulation.

2.10. FSO Communication System Design Specifications

The following are the design specifications of the combined FSO communication system, below this:

Table 2. FSO Communication System Design Specifications [11]

Design Parameters	Value
Bit Rate	1 Gps
Power	20 dBm
Frequency	1550 nm
Transmitter aperture diameter	10 cm
Receiver aperture diameter	30 cm
Link Range	1-5 km
Beam divergence	0.2 mrad
Detector gain	10
Responsivity	9
Attenuation	0.7 and 5 dB/km
Sequence length	128 bit

2.11. Results from Eye Diagram and Optical Spectrum Analyzer

The following is a comparison of the simulation results from eye diagrams with attenuation of 0.7 dB/km as well as bright weather conditions within 1 km using NRZ and RZ coding line, below this:

Figure 4. Graph of Comparison on Eye Diagrams in NRZ and RZ Line Coding

Figure 5 is a Graph of comparison on eye diagrams in NRZ and RZ Line Coding. In this graph the distance used is 1 km. In the picture above, the eye diagram of the NRZ line coding is more perfect than the eye diagram of the RZ

line coding. While figure 5 (a) and figure 5 (b) are the results of a graph of the comparison of the Optical Spectrum Analyzer using NRZ and RZ line coding with bright weather conditions at 1 km. This makes the results of the Optical Spectrum Analyzer characteristic of NRZ and RZ line coding.

Figure 5. (a) Graph of the Optical Spectrum Analyzer between wavelengths with power uses NRZ line coding in bright and rainy conditions at attenuation 0.7 and 5 dB/km, (b) Graph of the Optical Spectrum Analyzer between wave-length with power uses RZ line coding in bright and rainy conditions at attenuation 0.7 and 5 dB/km

2.12. Eye Height Graph Results

Figure 6 (a) and figure 7 (a) are two graphs of eye height in the NRZ line coding in bright weather conditions and rain with attenuation of 0.7 and 5 dB/km. Eye height is the result of one of the eye diagram graphs. In figure 6 (a) the highest amplitude is at eye height at 1 km, its maximum amplitude is 7.49 at 0.5 s. While in figure 7 (a) the highest amplitude is at eye height at 1 km, the maximum amplitude is 2.83 at 0.46 s.

Whereas figure 6 (b) and figure 7 (b) are graphs of eye height in the RZ line coding in bright weather conditions and rain with attenuation of 0.7 and 5 dB/km. In figure 6 (b), the highest amplitude is at eye height at 1 km, the maximum amplitude is 6.3 at 0.46 s. While in figure 7 (b) the highest amplitude is at eye height at 1 km, the maximum amplitude is at 2.34 at 0.46 s.

2.13. Results of Data Processing Comparison of NRZ with RZ Line Coding in Bright Weather

Figure 8 (a) is a graph of between received signal power with distance using NRZ and RZ line coding in bright conditions at attenuation of 0.7 dB/km. In figure 8 (a) NRZ line coding has a received signal power value greater than the RZ line coding at its highest point at 44.78 dBm and its lowest point at 16.61 dBm at a distance of 1 km and 5 km. While the RZ line coding is at its highest point at 40 dBm and its lowest point is at 11.89 dBm at a distance of 1 km and 5 km.

Figure 8 (b) is a graph of between the received photocurrent with distance using line coding NRZ and RZ in bright conditions at attenuation of 0.7 dB/km. In figure 8 (b) NRZ line coding has a received photocurrent value greater than the line coding RZ at its highest point at 4367.65 mA and its lowest point at 170.49 mA at a distance of 1 km and 5 km. While the RZ line coding is at its highest point at 2187.65 mA and its lowest point is at 85.39 mA at a distance of 1 km and 5 km.

(a)

(b)

Figure 6. (a) Graph of eye height on the NRZ line coding in bright weather conditions with attenuation of 0.7 dB/km, (b) Graph of eye height on the RZ line coding in bright weather conditions with attenuation of 0.7 dB/km.

(a)

(b)

Figure 7. (a) Graph of eye height on NRZ line coding in rainy weather conditions with attenuation of 5 dB/km, (b) Graph of eye height on RZ line coding in rainy weather conditions with attenuation of 5 dB/km

(a)

Figure 8. (a) Graph of between received signal power with distance using NRZ and RZ line coding in bright conditions at attenuation of 0.7 dB/km, (b) Graph of between received photocurrent with distance using NRZ and RZ line coding in bright conditions at attenuation of 0.7 dB/km.

2.14. Results of Data Processing Comparison of NRZ with RZ Line Coding in Rainy Weather

Figure 9 (a) is a graph of between received signal power with distance using NRZ and RZ line coding in rain conditions in attenuation 5 dB/km. In figure 9 (a) the NRZ line coding has the received signal power value greater than the RZ line coding at its highest point at 36.18 dBm and its lowest point at -26.38 dBm at a distance of 1 km and 5 km. While the RZ line coding is at its highest point at 31.47 dBm and its lowest point is -31.09 dBm at a distance of 1 km and 5 km.

In rainy conditions it has a decrease in the received signal power value to distance. NRZ line coding at a distance of 4 km received signal power decreased by more than 0 dBm which is -12.9 dBm. Meanwhile, in the RZ line coding, a distance of 3 km is received signal power which is -3.24 dBm. This is because the characteristics of the physical attenuation will be different in different weather conditions too. The attenuation value of bright weather conditions is smaller between 0.2-3 dB / km, while in rain conditions between 4-17 dB / km.

Figure 9 (b) is a graph of between the received photocurrent with distance using NRZ and RZ line coding in the rain conditions in attenuation 5 dB/km. In figure 9 (b) NRZ line coding has a received photocurrent value greater than the RZ line coding at its highest point at 1622.73 mA and its lowest point at 1.2 mA at a distance of 1 km and 5 km. While the RZ line coding is at its highest point at 812.79 mA and the lowest point is at 0.6 mA at a distance of 1 and 5 km.

2.15. Results of Data Processing Comparison of NRZ with RZ Line Coding in Bright and Rainy Weather

Figure 10 (a) is a graph of between received signal

power and distance using NRZ line coding in bright and rainy conditions at attenuation of 0.7 and 5 dB/km. In figure 10 (a) line coding NRZ bright conditions have a received signal power value greater than the NRZ coding line rain conditions at the highest point at 44.78 dBm and the lowest point at 16.61 dBm at a distance of 1 km and 5 km. Whereas NRZ rain conditions at the highest point at 36.18 dBm and the lowest point at -26.38 dBm at a distance of 1 km and 5 km.

Figure 10 (b) is a graph of between received signal power and distance using RZ line coding in bright and rainy conditions at attenuation of 0.7 and 5 dB/km. In figure 10 (b) line coding of RZ bright conditions has a received signal power value greater than the RZ coding line the condition of rain at its highest point at 40 dBm and the lowest point at 11.89 dBm at a distance of 1 km and 5 km. Whereas NRZ rain conditions at its highest point at 31.47 dBm and the lowest point at -31.09 dBm at a distance of 1 km and 5 km.

Figure 9. (a) Graph of between received signal power with distance using NRZ and RZ line coding in rain conditions in attenuation 5 dB/km, (b) Graph of between received photocurrent graphics with distance using NRZ and RZ line coding in rain conditions in attenuation 5 dB/km.

Figure 10. Graph of between received signal power with distance using NRZ line coding in bright and rainy conditions at attenuation 0.7 and 5 dB/km, (b) Graph of between received signal power with distance using RZ line coding in bright and rain conditions at attenuation 0.7 and 5 dB/km.

3. Conclusions

Based on the simulation results, it can be concluded that each NRZ and RZ line coding has its own characteristics, as seen from the results of different Eye Diagram and Optical Spectrum Analyzer diagrams. In the system, the FSO line coding NRZ has an eye height value, received signal power, and receives currents greater than the RZ line encoding at a distance of 1 km and 5 km in bright and rainy conditions. In the trial of this FSO communication system, it is better to use it at a distance of 1 km, because the received signal power is above 20 dBm and received photocurrent is still above 800 mA for NRZ and RZ line coding. This is because the weakening value of sunny weather conditions is smaller between 0.2-3 dB/km, while the weather conditions are between 4-17 dB/km.

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