A Processing–Microstructure Correlation in ZrB$_2$–SiC Composites Hot-pressed under a Load of 10 MPa

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Abstract Monolithic ZrB$_2$ ceramic and its composites, with 5 to 30 vol. % SiC, has been prepared by hot pressing at temperatures of 1700, 1850 and 2000 °C, for 30 minutes under relatively low pressure of 10 MPa. Densification behavior of ZrB$_2$-based composites is improved by the addition of SiC particulates. The fracture surface of monolithic ZrB$_2$ ceramics shows a grained structure, with faceted ZrB$_2$ grains, as the fracture appears to spread prevalently along an intergranular path. The ZrB$_2$/ZrB$_2$ boundary interface is seemingly free of any secondary phases. The microstructure of ZrB$_2$–30 vol. % SiC composite, hot-pressed at 1700 °C, is consistent with measured porosity for the sample that has ~8% open pores, nearly without closed pores. It seems that mechanical interlocking between ZrB$_2$ and SiC is an important mechanism for densification. In the microstructure of specimens consolidated at 1850 °C, neck formation between ZrB$_2$ particles is visible. In contrast, relatively fully dense samples are obtained by hot-pressing at 2000 °C. Intergranular SiC particles inside ZrB$_2$ grains show the occurrence of mass transfer among ZrB$_2$ particles, which in effect brings the elimination of pores to a fortunate ending. Efficient mixing of starting powders is very critical in order to achieve a fine-grained homogenous microstructure.

Keywords Hot Pressing, Zirconium Diboride, Silicon Carbide; Microstructure, Grain Growth, Powder Mixing

1. Introduction

Zirconium diboride is striking for its ultra-high melting temperature as well as its hardness, elastic modulus, low electrical resistivity, and resistance to chemical attack. As a result, this material has been proposed for a variety of structural applications at room and elevated temperature, including armor, cutting tools, molten metal containment, steel processing, and electrodes. Zirconium diboride is also considered to be an ultra-high-temperature ceramic and is a candidate to be used as leading edges and propulsion components in hypersonic aerospace vehicles and advanced reusable atmospheric reentry vehicles [1-3].
varied from 2.2 to 4.7 μm and 1.2 to 2.7, respectively [11]. The effect of SiC particle size, ranging from 0.45 to 10 μm, on the microstructure of ZrB₂-based composites, containing 30 vol. % SiC, was studied. Investigations showed that smaller starting SiC particles led to improved densification and finer microstructure [12]. A ZrB₂-based composite containing 20 vol. % nano-sized β-SiC particles (30 nm) was hot pressed at 1900 °C for 30 min under 30 MPa. It was shown that the grain growth of ZrB₂ matrix was effectively suppressed by SiC particles [13]. Recently, the dominant densification mechanisms for hot pressing of ZrB₂–20 vol. % SiC composite, at different sintering temperatures and pressures, was identified. For hot pressing at 1700 °C, it was found to be only mechanically driven particle fragmentation and rearrangement, whereas at 1850 °C a plastic flow mechanism started to happen. At 2000 °C, the dominant mechanism changed from plastic flow to grain boundary diffusion [14].

Although in recent years, ZrB₂-based composites have been densified by other techniques such as pressureless sintering [6, 15-17], reactive hot pressing [4, 9, 18-24], and spark plasma sintering [25-28], but hot pressing is still the dominant method in research on consolidation. Table 1 lists the compositions, starting particle sizes, sintering conditions, and relative densities of the composites investigated by researchers, employing hot pressing as the sintering method.

The purpose of this paper is to describe the microstructural conduct of ZrB₂–SiC composites, hot pressed under relatively low-pressure using mono-sized starting powders. X-ray diffraction analysis, optical microscopy and scanning electron microscopy micrographs are used to study the evolution of microstructure as a function of sintering temperature and SiC content. In addition, the densities and porosities of composites consolidated at 1700, 1850 and 2000 °C will be compared to deduce the effect of processing temperature.

### Table 1. Hot pressing conditions and relative densities of ZrB₂–SiC composites.

<table>
<thead>
<tr>
<th>Composition (vol. %)</th>
<th>Particle size (μm)</th>
<th>Hot pressing conditions</th>
<th>Relative density (%)</th>
<th>References</th>
</tr>
</thead>
<tbody>
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<td>ZrB₂</td>
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<td>ZrB₂</td>
<td>SiC</td>
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<tr>
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<td>20</td>
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<td>2000</td>
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<td>1900</td>
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<tr>
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<tr>
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<td>6</td>
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2. Experimental Procedure

2.1. Processing

ZrB$_2$ (particle size ~2 μm, purity ~99.9%, Leung Hi-tech Co., China) and α-SiC (particle size ~2 μm, purity >99%, Carborundum Universal Limited, India) powders were the starting materials. Powder samples of ZrB$_2$ with 0, 5, 10, 15, 20, 25 and 30 vol.% SiC were mixed at 120 rpm for 1 hour in a zirconia cup with balls. To investigate the effect of mixing on final microstructure of the composites, some samples were prepared without efficient mixing. Then, samples were loaded into a graphite die and boron nitride spray was applied to all graphite surfaces. Hot pressing was completed in a graphite resistance-heated vacuum hot press furnace (made by Shenyang Weitai Science & Technology Development Co., Ltd., China). In each hot pressing experiment, 10 MPa pressure was applied as soon as the final isothermal temperature cycle started. Samples were initially heated at a rate of 12 °C/min up to 1000 °C, given a dwell isotherm at 1000 °C for 30 min in order to remove volatile species from the powder batch, then heated again at a rate of 10 °C/min up to the designated temperatures. Above 1000 °C, the temperature of the graphite die was monitored using an infrared temperature sensor (Model IT-6). Hot pressing was carried out at different temperatures (1700, 1850 and 2000 °C), given a dwell isotherm for 30 min. Finally, the hot press furnace was cooled down naturally. One billet, with a diameter of 25 mm and thickness of 5 mm, was prepared for each experiment.

2.2. Characterization

X-ray diffraction (XRD) analysis (Cu lamp, λ = 1.54 Å, 40 kV, 30 mA, Siemens D5000 model) was carried out on the samples. Bulk density of samples was measured using the Archimedes’ technique with distilled water as the immersing medium, and the relative density was calculated with respect to theoretical density. The theoretical density was estimated using rule of mixtures, based on starting compositions of the samples and pure component densities ZrB$_2$: 6.1 g/cm$^3$ and SiC: 3.2 g/cm$^3$. Microstructure characterization was carried out by an optical microscopy (Nikon, Eclipse MA100, Japan), beside a scanning electron microscopy (Mira3 Tescan, Czech Republic). Chemical analysis was performed simultaneously with SEM, using energy dispersive spectroscopy (EDS). Samples were prepared for microscopy by a four-step mechanical polishing to 0.25 μm, using diamond abrasive. Some of the polished sections were thermally etched at 1600 °C for 30 min. The grain size was determined from optical microscopy images, using image analysis software (ImageJ 1.44p, Wayne Rasband, National Institute of Health, USA), after thermal etching in vacuum (5×10$^{-2}$ Pa) at 1600 °C for 30 min.

3. Results and Discussion

Fig. 1 presents the SEM images of morphologies and the XRD of starting materials. As it seems, the only crystalline phases detected were ZrB$_2$ and SiC. As shown in Fig. 2, the densities decreased with increasing SiC content, due to lower density of SiC than ZrB$_2$ and/or decreasing hot pressing temperature and consequent incomplete densification. Based on this figure, it seems that by densification at 2000 °C, the theoretical and experimental values are meeting each other in the ZrB$_2$–30 vol.% SiC composite.
Densification behavior of ZrB₂-based composites were improved by adding SiC particulate. The monolithic ZrB₂ ceramic and the composites which have been reinforced using inadequate SiC particulates, demonstrated a sinterability lower than that of appropriate composite samples. Contamination of ZrB₂ powder by oxygen supports evaporation-condensation and grain coarsening mechanisms during hot pressing, which exacerbates the maximum reachable density. Achieving a denser composite with increasing additive content, manifestly confirmed the advantageous role of SiC in restricting such harmful mechanisms for densification. It seems that the cleaning of ZrB₂ powder surface from oxygen, through chemical interactions with SiC, is a key step to acquire fully dense materials.

The fracture surface of monolithic ZrB₂ ceramics, densified at 1850 and 2000 °C, were examined by SEM (Fig. 4). A grained structure with faceted ZrB₂ grains has been shown, as the fracture appeared to spread prevalently along an intergranular path. The ZrB₂/ZrB₂ boundary interfaces were seemingly free of secondary phases. Some pores were visible in the SEM micrographs of monolithic ZrB₂ ceramic, sintered at 1850 °C (Fig. 4-a), that had a relative density of ~89 %. On the other hand, since the relative density had been measured to be about 97 %, no discernible porosity was found in the hot pressed sample at 2000 °C (Fig. 4-b).

Examination of ZrB₂–SiC composite by SEM showed that SiC particles were dispersed in the ZrB₂ matrix. The microstructure of ZrB₂–30 vol. % SiC composite, hot pressed at 1700 °C, is shown in Fig. 5. It is consistent with

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**Figure 2.** Density of hot pressed ZrB₂–SiC composites at different temperatures for 30 min under 10 MPa load.

**Figure 3.** Amount and type of porosities in hot pressed ZrB₂–SiC composites at different temperatures.

**Figure 4.** SEM micrographs of fracture surfaces of monolithic ZrB₂ ceramics, hot pressed at different temperatures; (a) 1850 °C, and (b) 2000 °C.
measured porosity value for the sample that has more than 8 percent open pores nearly without closed pores. It seems that mechanical interlocking between ZrB$_2$ and SiC is an important mechanism for densification at 1700 °C.

In the microstructure of monolithic ZrB$_2$ and ZrB$_2$–30 vol. % SiC composite, after hot pressing at 1850 °C (Fig. 6), neck formation between ZrB$_2$ particles in both samples was observed. There were more obvious grain boundaries between ZrB$_2$ and SiC in the composite sample. It seems that the density of ZrB$_2$–30 vol. % SiC composite is higher than that of monolithic ceramic, hot pressed in the same condition. This is in agreement with the result of porosity curve versus SiC addition (Fig. 3), because the amount of porosity in the composite sample is three times less than the other one. However, by the formation of necks, the density increased after hot pressing at 1850 °C in all compositions in comparison with samples processed at 1700 °C (as shown in Fig. 2). A highly dense network of dislocations in ZrB$_2$ grain was found by Patel et al. [14] in TEM images of a sample hot pressed at 1850 °C under 25 MPa. Limited grain growth and a network of dislocations in the sample suggested that the dominant densification mechanism might be plastic deformation of ZrB$_2$ grains.

In contrast, relatively fully dense samples were obtained by hot pressing at 2000 °C. SEM observations of the polished sections (Fig. 7) confirmed that residual porosity is not substantial.

The XRD analysis (not shown here) from fully dense composites, except ZrB$_2$ and SiC, did not detect any extra crystalline phases. Patel et al. have shown a considerable grain growth and extinction of dislocations in a sample hot pressed at 2000 °C, and therefore, grain boundary diffusion could be the dominant densification mechanism. The ruin of dislocations at interfaces may be due to the diffusion of
atoms through grain boundaries [14]. Intergranular SiC particles inside ZrB₂ grains (Fig. 8 and Fig. 10) prove a meaningful mass transfer among the ZrB₂ particles, which in effect brought the elimination of the pores to a fortunate ending.

Average ZrB₂ grain sizes in the samples (consolidated at 2000 °C) were measured from the polished and thermally etched surfaces (Fig. 8). As the results are shown in Fig. 9, largest grain sizes belonged to monolithic ZrB₂ ceramic (~15.4 μm). For the composite samples, average ZrB₂ grain size reached ~3.5 μm, when 30 vol. % SiC was added to the ZrB₂ powder under the same conditions. Hence, the effect of SiC as a ZrB₂ grain growth controller is demonstrated clearly.

The influence of inefficient mixing of the starting powders on the final microstructure of the composites has been revealed in Fig. 10. In the optical microscope images of the polished and thermally etched surfaces of nearly fully dense (but without proper mixing) ZrB₂-based composites, there is a clear boundary that has divided the microstructure into two regions. In the region with relatively good distribution of SiC phase, the ZrB₂ grains seem to have normal size (based on Fig. 9), but on the other side, ZrB₂ grains grow dramatically due to lack of SiC phases, reaching a microstructure like monolithic ZrB₂ ceramic. Therefore, efficient mixing of the starting powders is very critical in order to achieve a fine-grained homogenous microstructure.

**4. Conclusions**

The effect of consolidating temperature and SiC content as a reinforcement on the microstructure of hot pressed ZrB₂–SiC composites under 10 MPa was investigated. Increasing the amount of SiC particles and using higher sintering temperatures enhanced the densification of ZrB₂–SiC composites, reaching a fully dense sample by hot pressing at 2000 °C for ZrB₂-based composite, containing 30 vol. % SiC.
The microstructure of composites is consistent with measured values for porosity. Mechanical interlocking between ZrB₂ and SiC, neck formation between ZrB₂ particles alongside with more obvious grain boundaries between ZrB₂ and SiC, and Intergranular SiC particles inside ZrB₂ grains was observed in the microstructures of composites densified at 1700, 1850, and 2000 °C, respectively. Achieving a finely grained homogenous microstructure was strongly depended on an efficient mixing of the starting powders.

![Figure 10. Optical microscope images of polished and thermally etched surfaces of ZrB₂-based composites, hot pressed at 2000 °C; (a) ZrB₂–20 vol. % SiC, and (b) ZrB₂–30 vol. % SiC (Light grains are ZrB₂ and dark grains are SiC).](image)

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### REFERENCES


